

# 4.401/4.464 Environmental Technologies in Buildings

Christoph Reinhart

4.401 Thermal Comfort and Case Studies

# Future Climate Files

# Bioclimatic Design

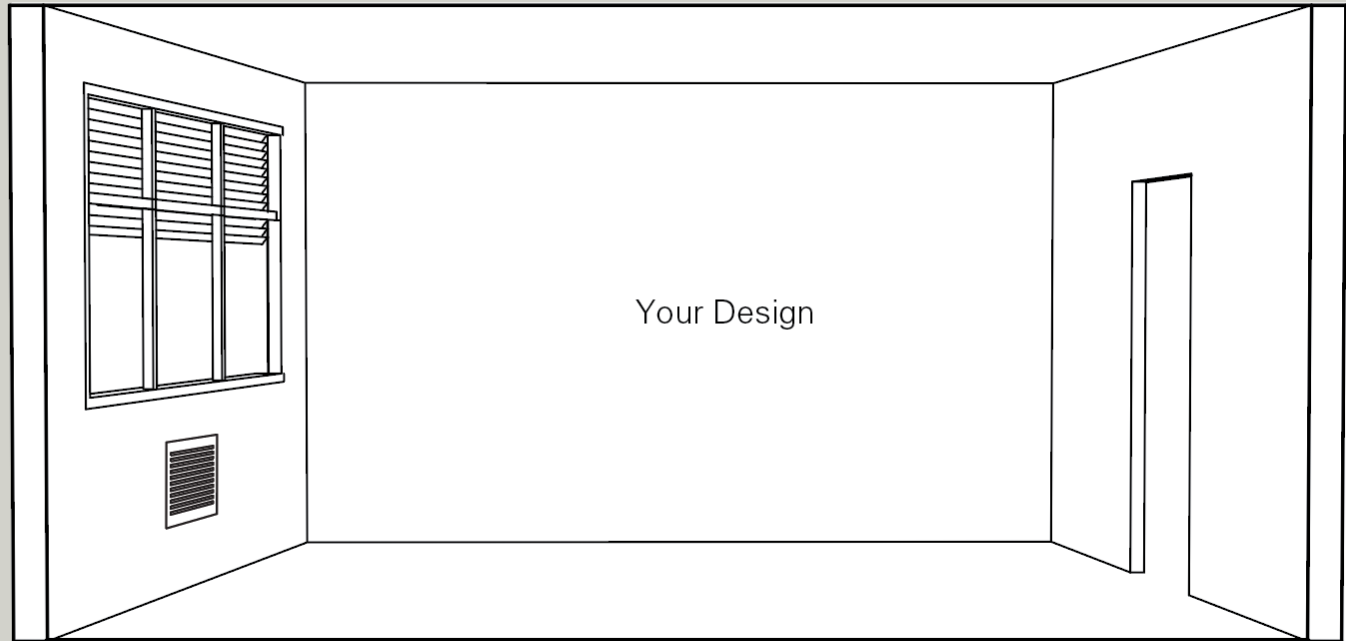
Solar Radiation

Temperature

Relative Humidity

Wind direction

Wind speed



For a thermal analysis of a building we need local hourly climate data from a weather file including direct and diffuse solar radiation, wind speed and direction, as well as temperature and relative humidity.

# Historic Weather Fluctuations and Resulting Building Energy Use

See Figures 3-9 and 3-10, Drury B. Crawley, "Building Performance Simulation: A Tool for Policy Making," PhD thesis, University of Strathclyde, 2008 (PDF).

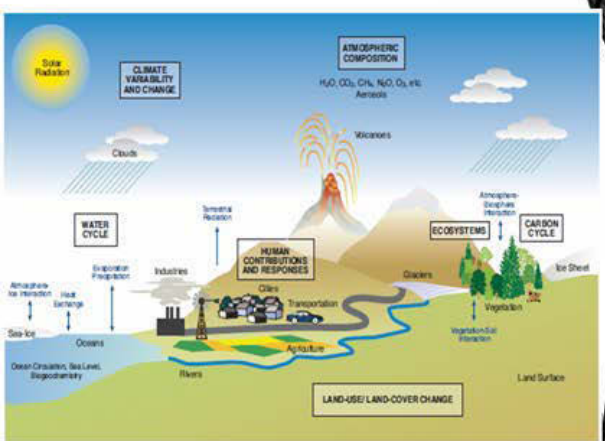
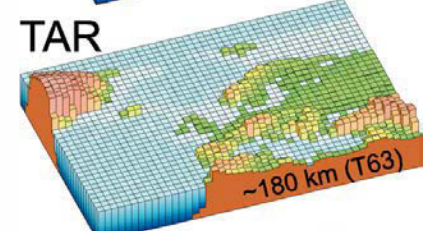
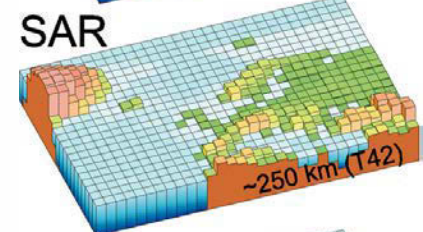
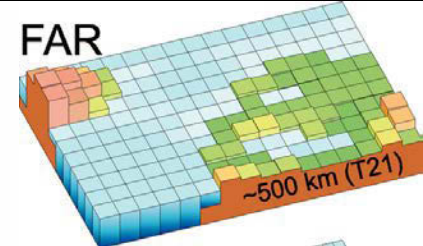
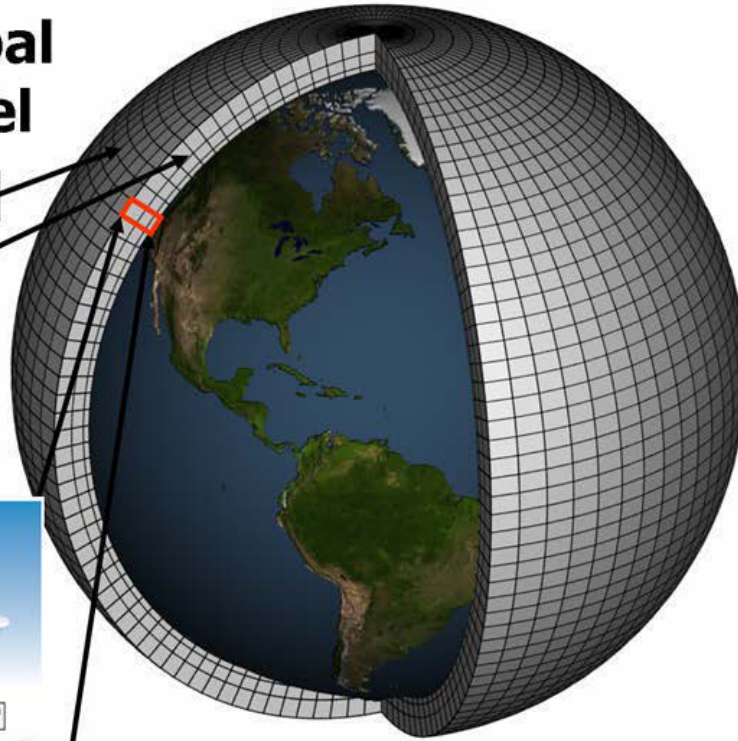
*How can we consider climate  
change in our designs?*

# Future Climate Files

## Schematic for Global Atmospheric Model

Horizontal Grid (Latitude-Longitude)

Vertical Grid (Height or Pressure)



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# Climate Change Weather File Generator

<http://www.energy.soton.ac.uk/ccworldweathergen/>

Generates future climate files for locations worldwide (with limitations) with a specific focus on the UK. It is based on the 'morphing' methodology.

Belcher SE, Hacker JN, Powell DS. "Constructing design weather data for future climates." *Building Services Engineering Research and Technology* 2005; 26 (1): 49-61.

7 Jentsch MF, Bahaj AS, James PAB. "Climate change future proofing of buildings - Generation and assessment of building simulation weather files." *Energy and Buildings* 2008; 40 (12): 2148-2168.

# Climate Change Weather File Generator

**CCWorldWeatherGen climate change weather file generator V1.5** [manual](#)  
 For transforming EPW weather files into climate change TMY2/EPW files. (Acknowledgements & disclaimer of warranties below)

Specify the HadCM3 data file path:

Summary of combined HadCM3 A2 ensemble climate change predictions for the selected weather site

**Selected scenario: A2 scenario ensemble for the 2080's**

		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	ANN
Daily mean temperature	<b>TEMP</b> (°C)	4.10	4.43	4.16	4.32	4.73	4.95	5.81	5.84	5.50	5.09	4.43	3.97	4.78
Maximum temperature	<b>TMAX</b> (°C)	3.92	4.48	4.30	4.07	4.76	5.56	6.46	6.07	5.36	4.79	4.48	4.08	4.86
Minimum temperature	<b>TMIN</b> (°C)	4.39	4.56	3.83	4.42	4.77	4.62	5.52	5.88	5.68	5.27	4.30	4.02	4.77
Horizontal solar irradiation	<b>DSWF</b> W/m <sup>2</sup>	-3.96	-6.05	-4.22	-0.51	11.77	17.59	14.20	10.09	11.50	6.57	-1.14	-2.35	4.46
Total cloud cover	<b>TCLW</b> % points	-0.25	-0.50	-0.88	-0.13	-2.00	-3.00	-5.25	-5.00	-5.63	-4.38	-0.63	-0.88	-2.38
Total precipitation rate	<b>PREC</b> %	13.41	22.11	24.97	28.96	14.52	6.39	12.84	24.38	-8.16	2.82	12.59	15.63	14.21
Relative humidity	<b>RHUM</b> % points	-2.59	-4.54	-4.91	-3.85	-5.21	-7.54	-7.09	-4.63	-4.16	-3.27	-3.17	-3.15	-4.51
Mean sea level pressure	<b>MSLP</b> hpa	-1.61	-1.02	-2.48	-0.52	-1.22	-1.68	-2.09	-2.54	-1.09	-0.87	-0.21	-0.95	-1.36
Wind speed*	<b>WIND</b> %	-1.40	-2.22	0.70	-0.58	-1.41	-2.39	-1.79	-7.25	-6.52	-5.72	-1.20	-2.52	-2.69

\* Please note that wind speed resides on a 96x72 grid whilst all the other data is on a 96x73 grid

---

EPW weather file selection

**(1) Please specify the EPW file you want to transform**

Select EPW File for Morphing

**Current EPW baseline weather file for morphing:**

Baltimore Blt Washngtn Intl *Latitude:* 39.17 N  
*Longitude:* ##### W  
*Elevation:* 45 m

HadCM3 scenario timeframe selection

**(2) Please select a HadCM3 A2 scenario ensemble timeframe**

2020s  2050s  2080s

**Closest four HadCM3 96x73 grid points to Baltimore Blt Washngtn**

	<i>Latitude:</i>	<i>Longitude:</i>
<b>A</b>	40.00 N	##### W
<b>B</b>	40.00 N	##### W
<b>C</b>	37.50 N	##### W
<b>D</b>	37.50 N	##### W

**A2 scenario for the 208**

---

EPW weather file morphing

**(3) Click button to start morphing procedure**

Start Morphing Procedure

**Current morphed EPW weather file:**

Morphed EPW file for: Baltimore Blt Washngtn Intl, USA  
 HadCM3 A2 emissions senario ensemble for the 2080's

EPW/TMY2 weather file generation

**(4) Click the appropriate button for EPW / TMY2 file generation**

Generate Climate Change EPW Weather File

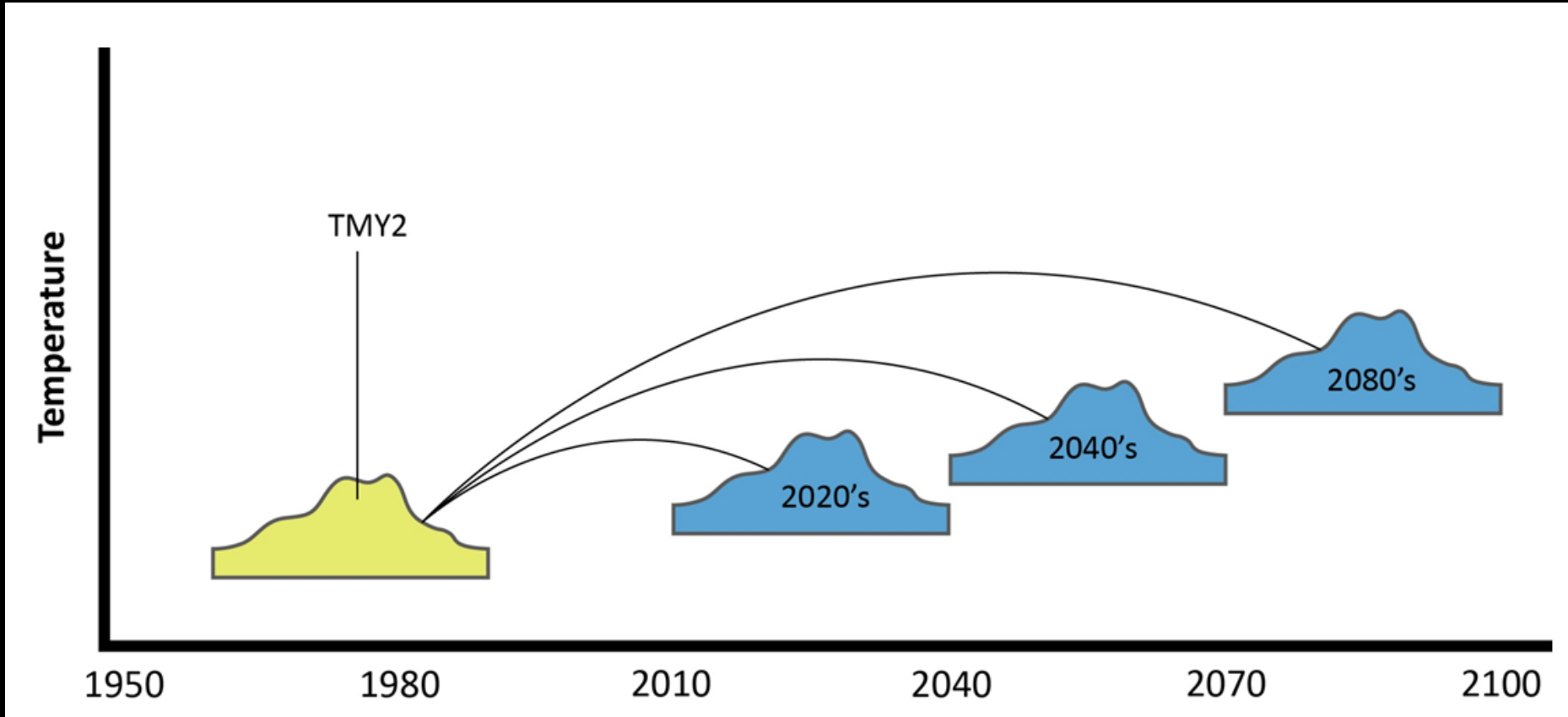
Generate Climate Change TMY2 Weather File

*To create a TMY2 file of the original EPW file click the button below:*

Generate Present-Day TMY2 Weather File form EPW data



# TMY2 Into The Future



# How large is the effect?

Harvard University – Gund Hall



DesignBuilder model

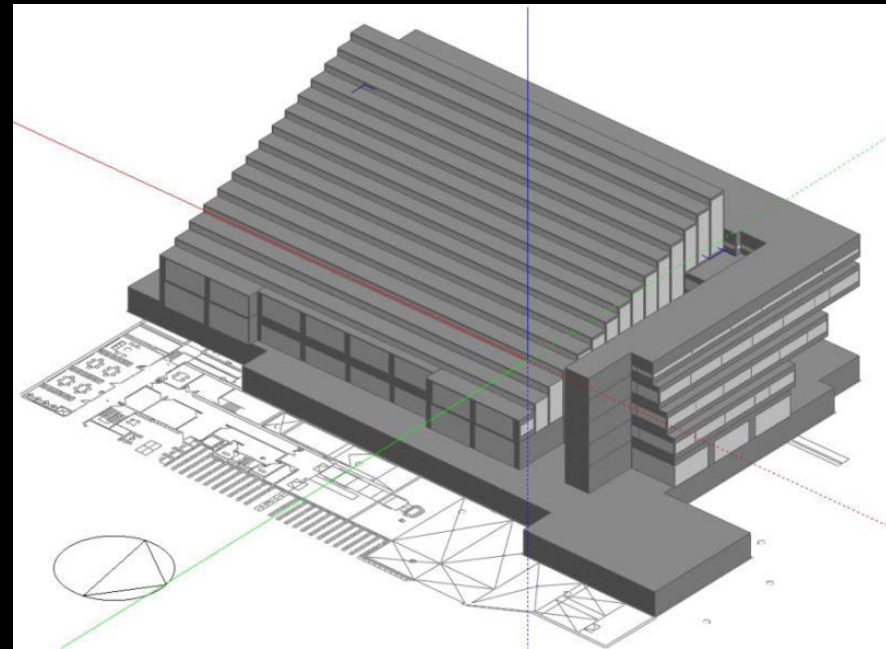
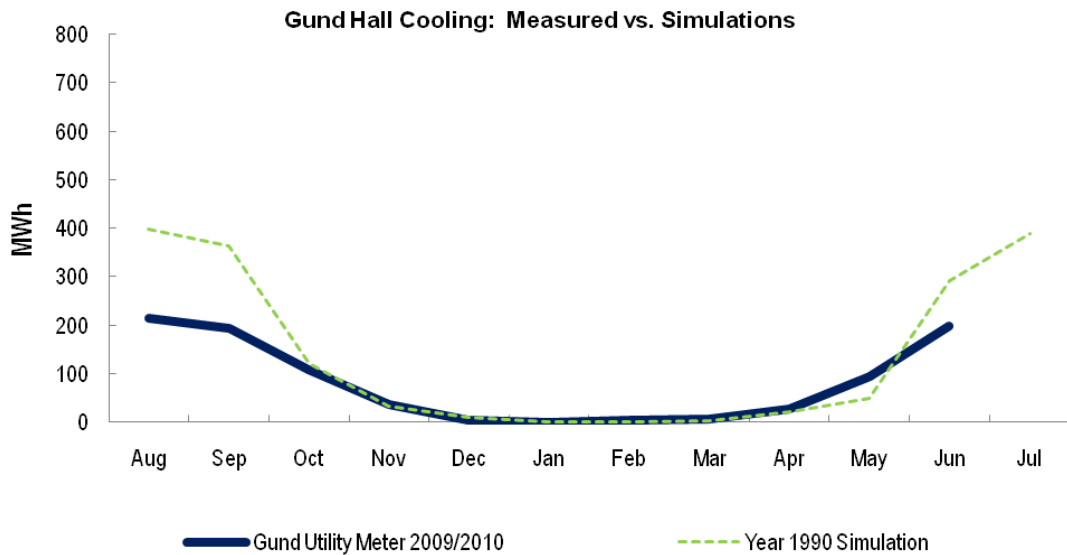
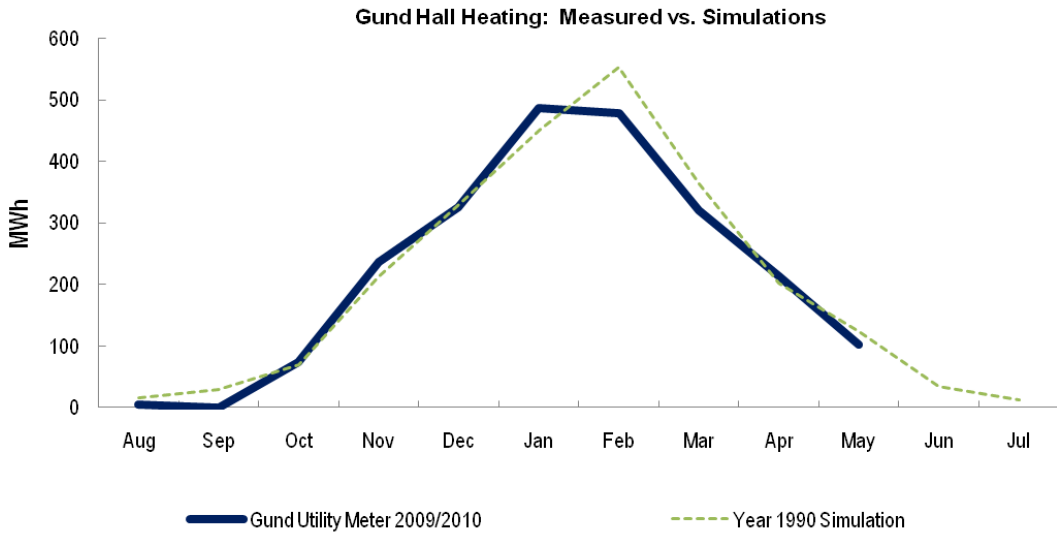


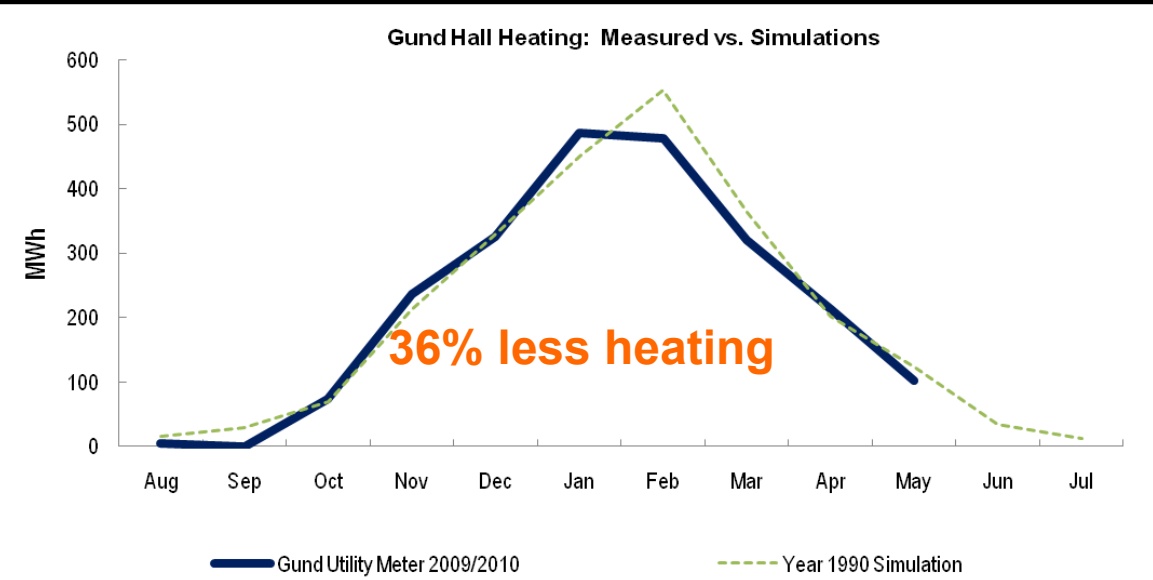
Photo © Harvard Graduate School of Design. All rights reserved. This content is excluded from our Creative Commons license. For more information, see <https://ocw.mit.edu/help/faq-fair-use/>.

# Gund Hall now

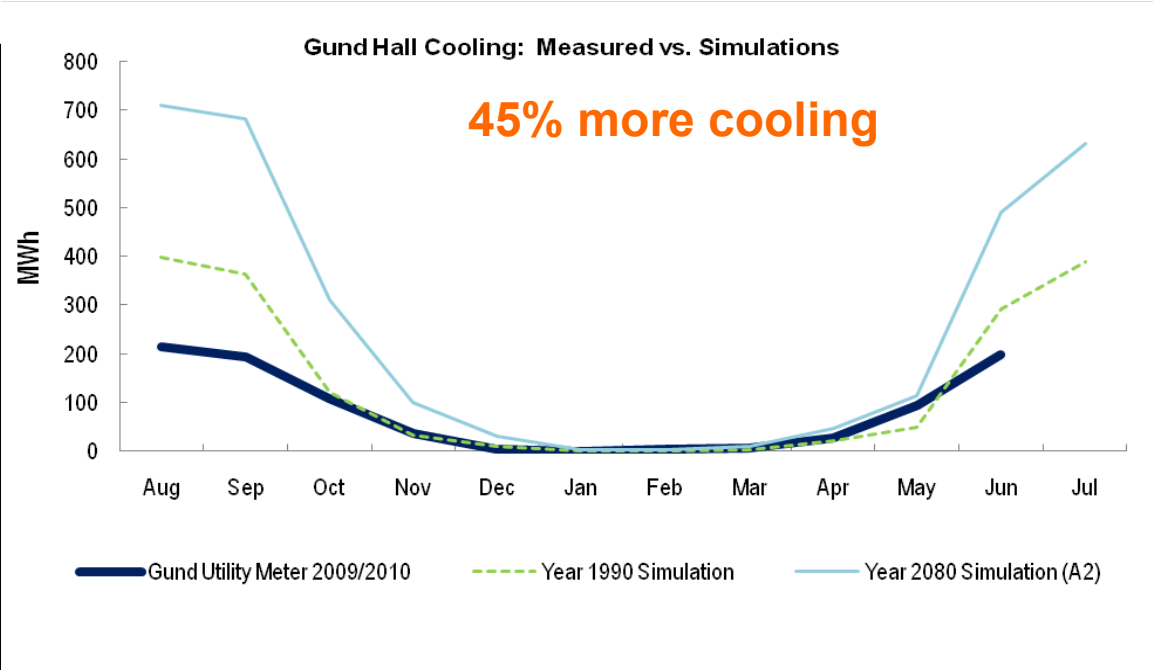
- 33 Zone E+ model
- 1990 TMY2 weather data for Boston



# Case Study I : Gund Hall now and then



- 33 Zone E+ model
- 1990 TMY2 weather data for Boston
- predicted 2080 weather data for the IPCC A2 scenario (medium to high emissions scenario).



# Microclimate

Local microclimate

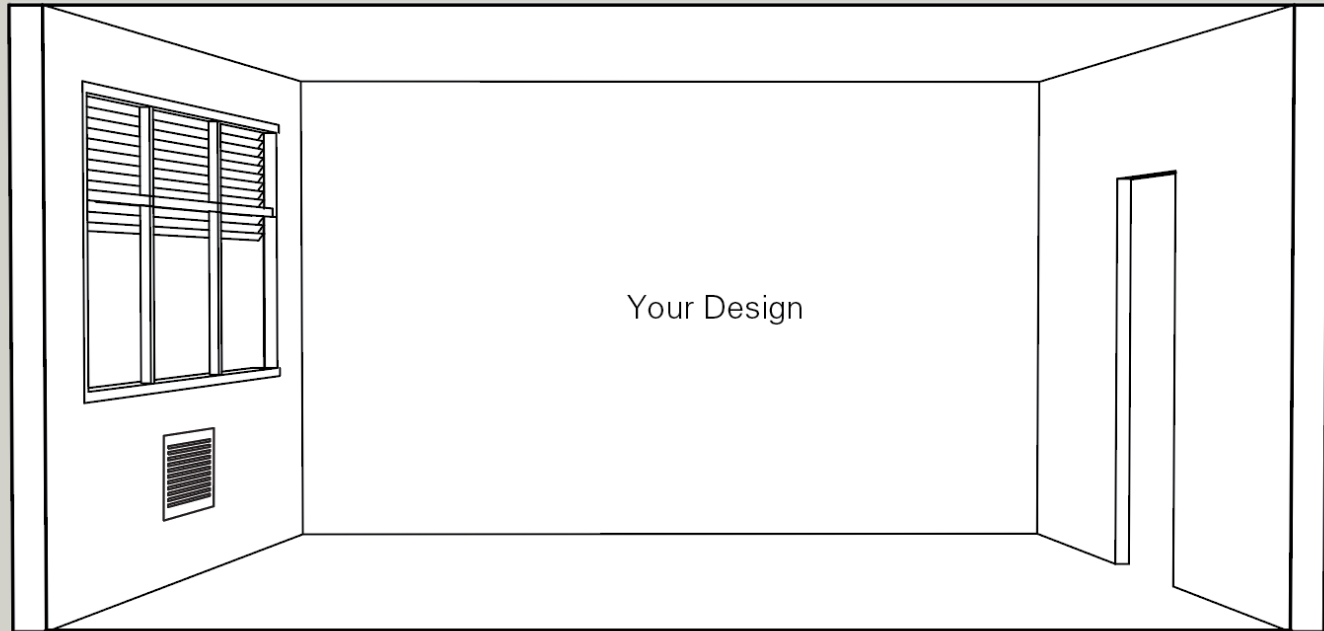
Solar Radiation

Temperature

Relative Humidity

Wind direction

Wind speed



You should also consider local microclimatic conditions:

- ❑ Local shading is considered by all major thermal simulation programs
- ❑ Other microclimatic effects are climate change, urban heat island, and local wind patterns.

# Climate Consultant

# Boston

**LOCATION:** Boston Logan Intl. Arpt, MA, USA  
**Latitude/Longitude:** 42.37° North, 71.02° West, **Time Zone from Greenwich** -5  
**Data Source:** TMY3 725090 WMO Station Number, **Elevation** 6 m

## MONTHLY DIURNAL AVERAGES

### LEGEND

#### HOURLY AVERAGES

##### TEMPERATURE: (degrees C)

- DRY BULB MEAN
- WET BULB MEAN
- DRY BULB (hourly)
- COMFORT ZONE

##### RADIATION: (Wh/sq.m)

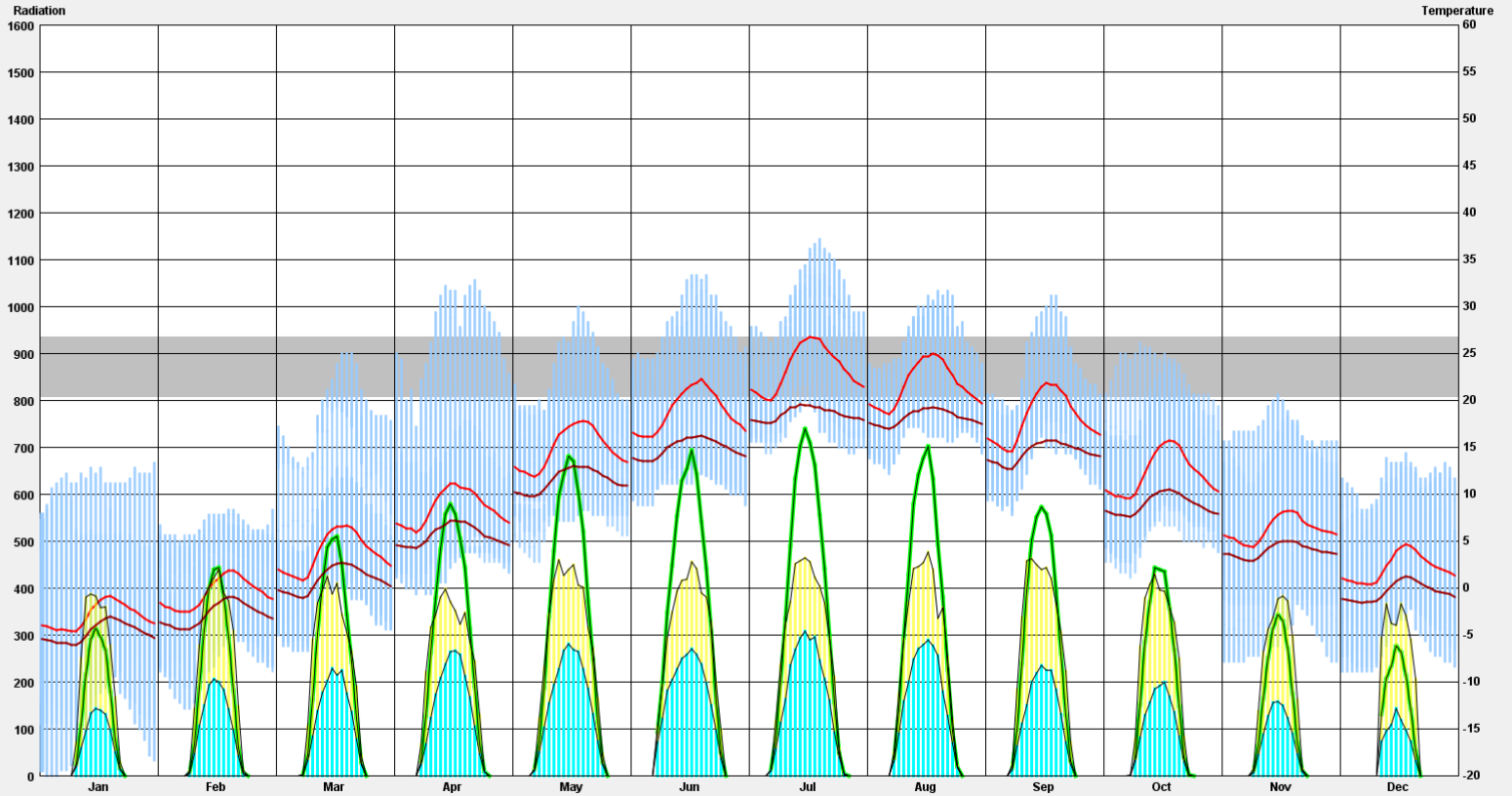
- █ GLOBAL HORIZ
- █ DIRECT NORMAL
- █ DIFFUSE

Display Hourly Dry Bulb Temp

##### TEMPERATURE RANGE:

-10 to 40 °C

Fit to Data



# Boston

**LEGEND**

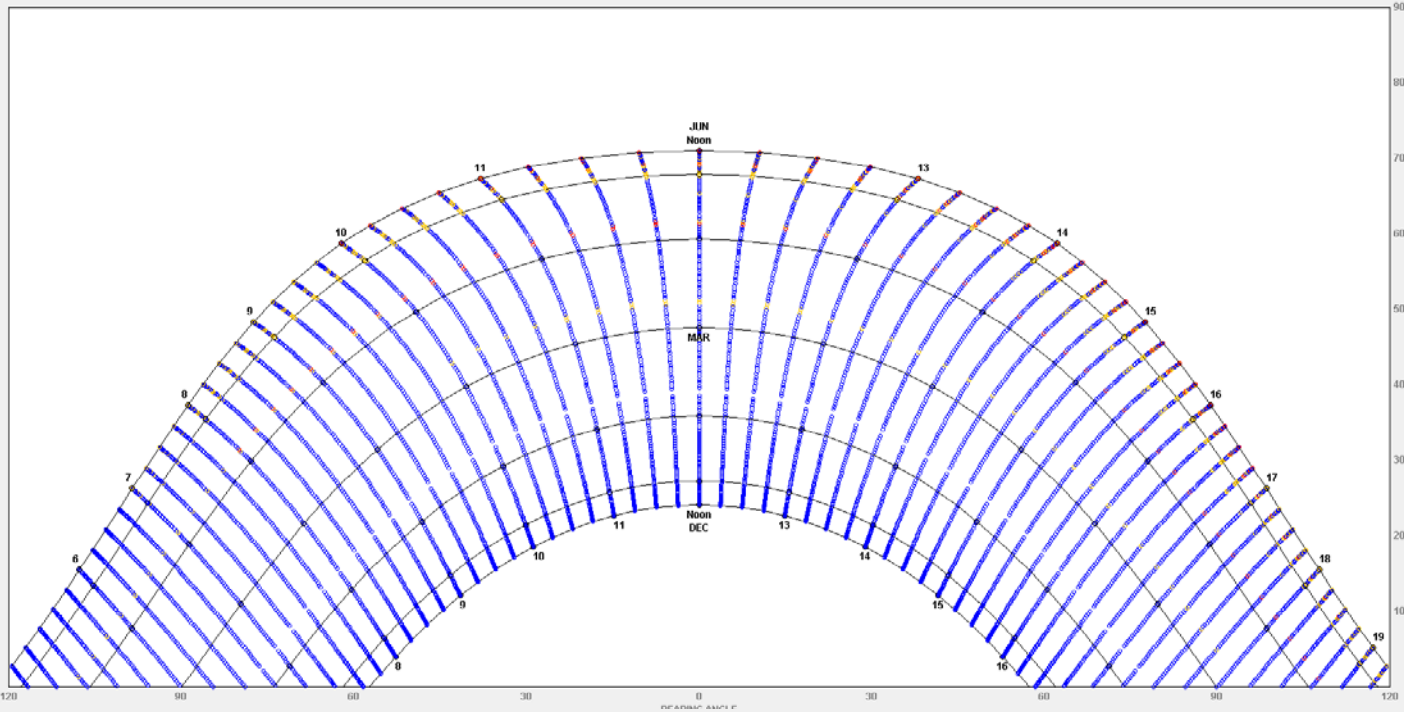
- ◊ **WARM/HOT > 27°C**  
(SHADE NEEDED)  
84 Hours Exposed  
0 Hours Shaded
- ◊ **COMFORT > 20°C**  
(SHADE HELPS)  
200 Hours Exposed  
0 Hours Shaded
- ◊ **COOL/COLD < 20°C**  
(SUN NEEDED)  
2166 Hours Exposed  
0 Hours Shaded

**PLOT MONTHS:**

WINTER SPRING  
 December 21 to June 21

SUMMER FALL  
 June 21 to December 21

Display Grid  
 Display Shading Calculator  
 Display Obstruction Elevation  
 Input Obstructions



**LEGEND**

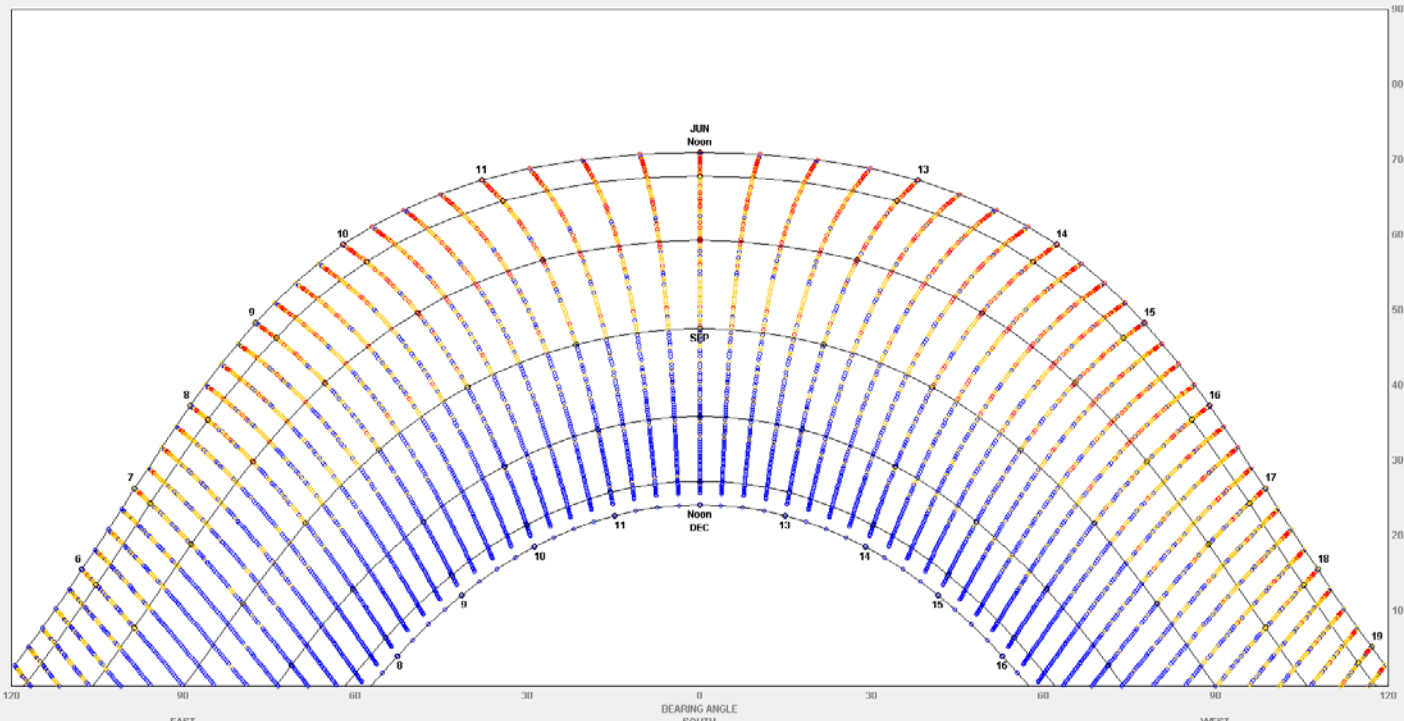
- ◊ **WARM/HOT > 27°C**  
(SHADE NEEDED)  
84 Hours Exposed  
0 Hours Shaded
- ◊ **COMFORT > 20°C**  
(SHADE HELPS)  
260 Hours Exposed  
0 Hours Shaded
- ◊ **COOL/COLD < 20°C**  
(SUN NEEDED)  
2166 Hours Exposed  
0 Hours Shaded

**PLOT MONTHS:**

WINTER SPRING  
 December 21 to June 21

SUMMER FALL  
 June 21 to December 21

Display Grid  
 Display Shading Calculator  
 Display Obstruction Elevation  
 Input Obstructions





# Boston

## LEGEND

DRY-BULB TEMP (degrees C)

- 14% ■ < 0
- 66% ■ 0 - 21
- 16% ■ 21 - 27
- 4% ■ 27 - 38
- 0% ■ > 38

LOT: DRY-BULB TEMP

Hourly  Daily Min/Max

All Hours  Selected Hours

a.m. through midnight

All Months  Selected Months

JAN through DEC

One Month JAN Next Month

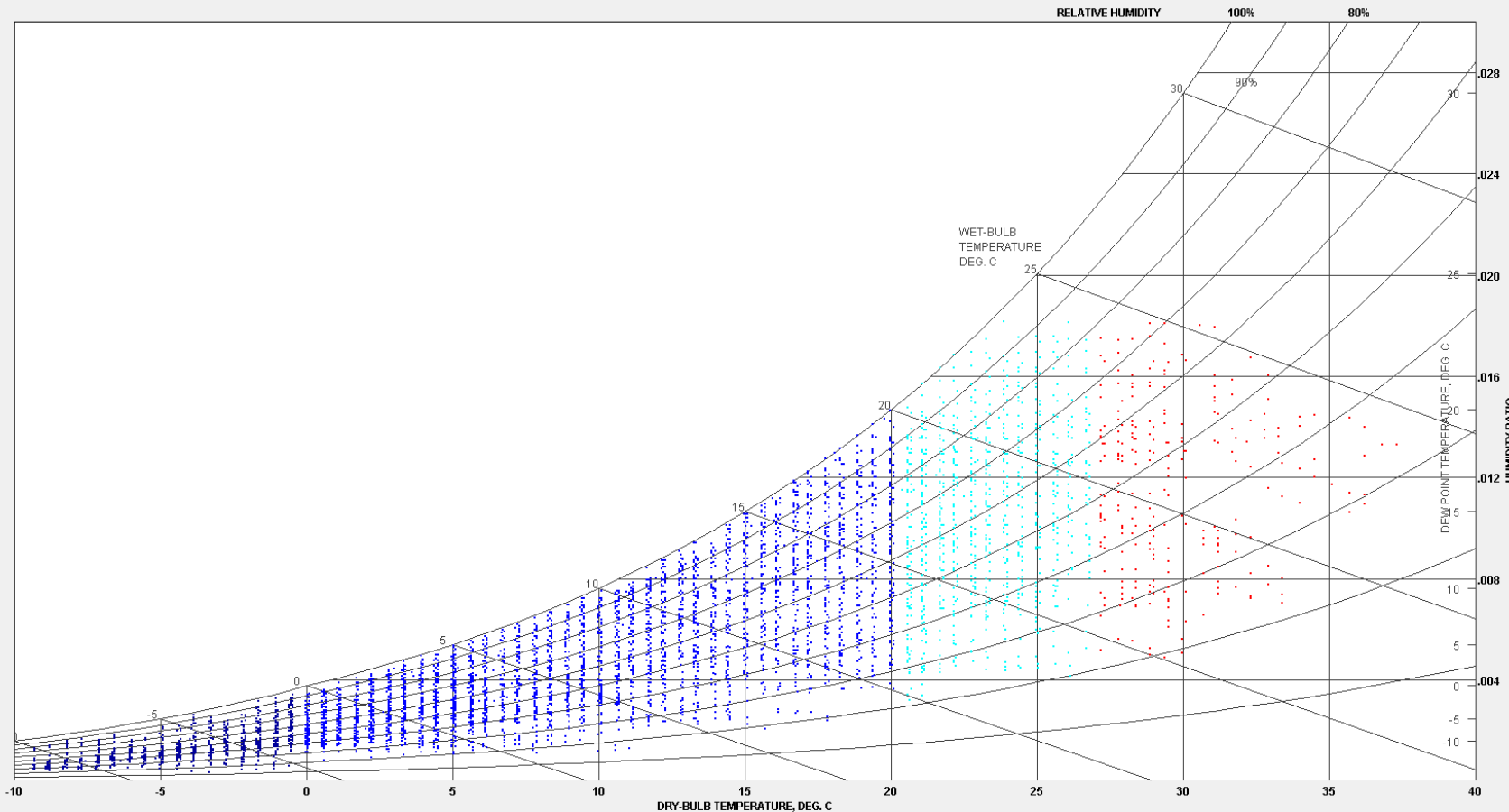
One Day 1 Next Day

TEMPERATURE RANGE:

-10 to 40 °C  Fit to Data

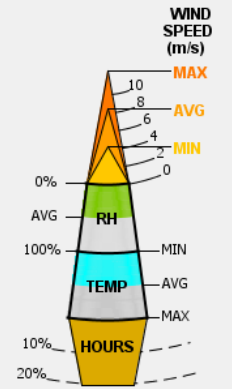
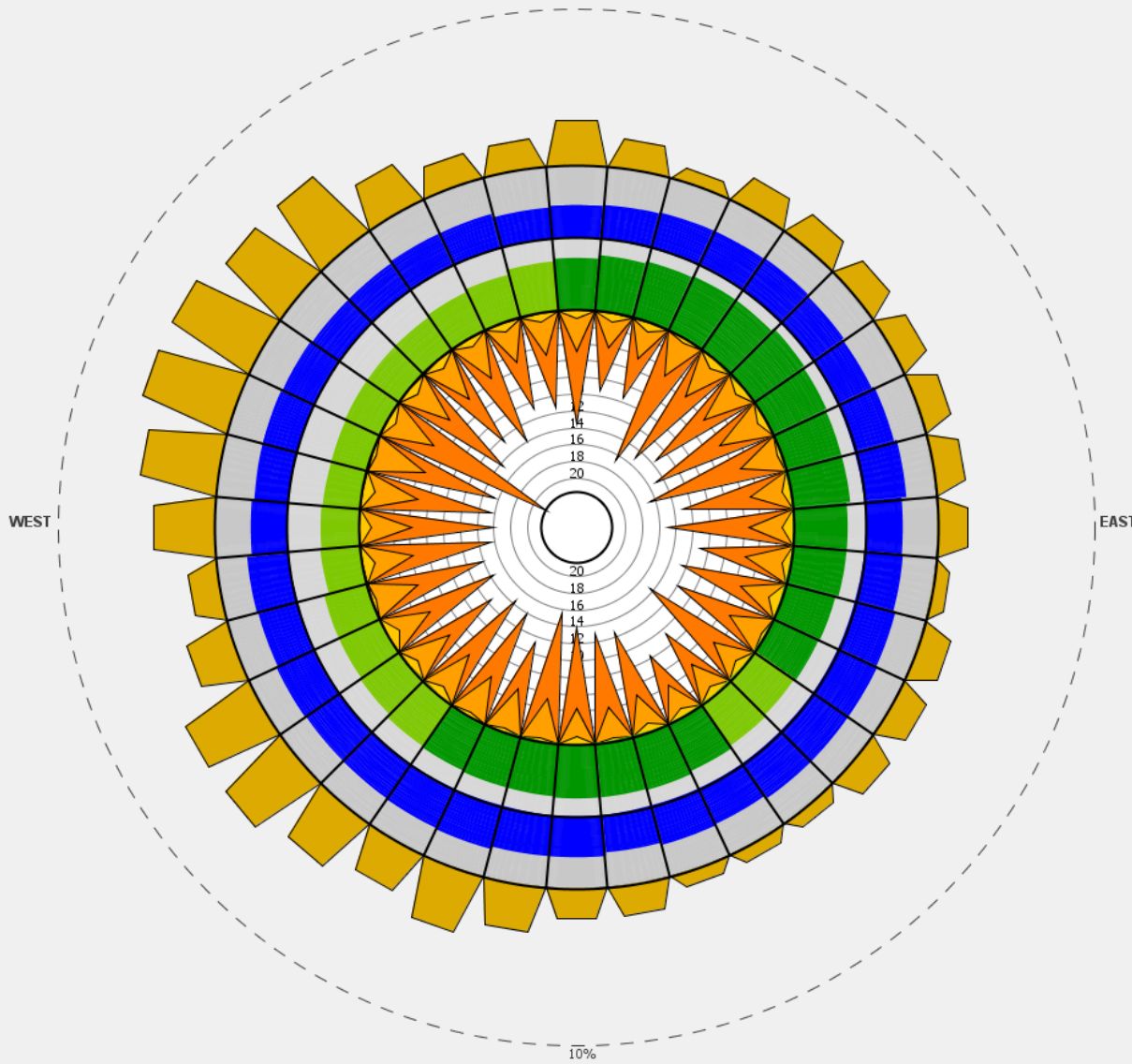
Display Design Strategies

Show Best set of Design Strategies

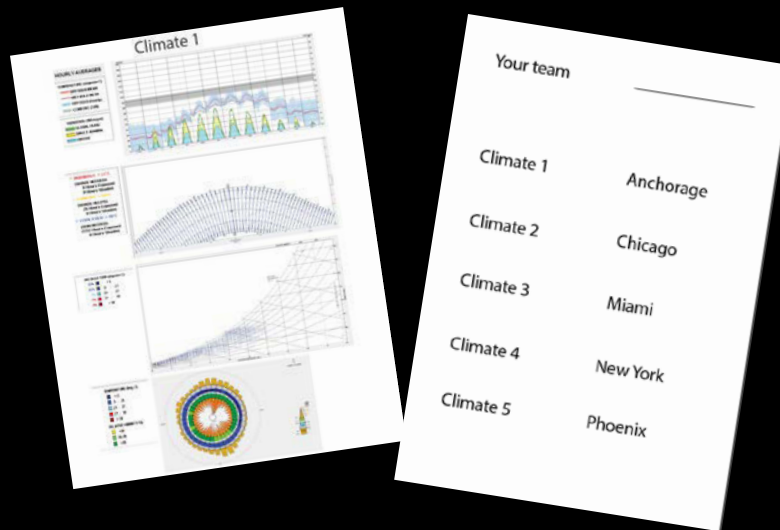


# Boston

N  
↑  
JANUARY - DECEMBER



## Climate File Board Game



# Climate File Board Game



# Thermal Comfort

*How much of our time do we spend  
indoors?*

Over 90%.

# Thermal Comfort - History

- ❑ Baldwin 1898: “It is usual to maintain a room temperature of 70° F.”
- ❑ Le Corbusier: “Maintain 18° C in buildings all over the world.”
- ❑ While temperature was early recognized to have a strong (the only) impact of thermal comfort, relative humidity was not a recognized concept. Instead, researchers used other descriptors such as stuffiness, smell, draught.
- ❑ This was partly due to our inability at the time to measure CO<sub>2</sub> or relative humidity.



# Migration and Adaptation

Human Migration Map: Route Summary Route Highlights

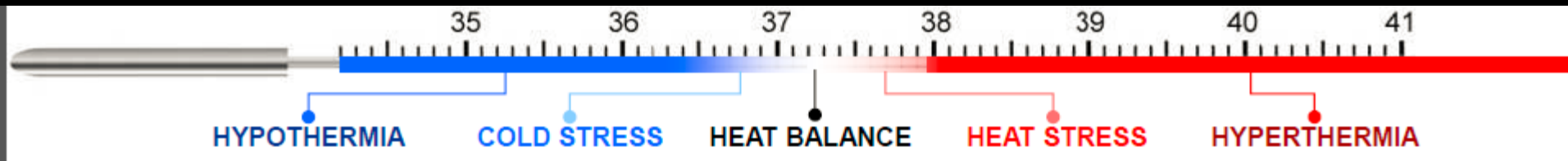


Top: map © National Geographic Partners, LLC. All rights reserved. This content is excluded from our Creative Commons license. For more information, see <https://ocw.mit.edu/help/faq-fair-use/>.  
Left: public domain photo courtesy of [Library of Congress](#).  
Center: public domain photo courtesy of [National Parks Service](#). Right: photo by instructor.



# Thermal Sensation - Regulation

Humans and many other mammals have efficient internal temperature regulating systems that automatically maintain stable core body temperatures at about 37.0° C. Individual differences in metabolism, hormone levels, physical activity can cause a variation of 0.6° C.



Basal metabolic rate +  
Muscular activity +  
Dietary intake  
Vasoconstriction  
Postural changes  
Adjust clothing level

Basal metabolic rate -  
Muscular activity -  
Drink cool fluids  
Thermal sweating  
Vasodilation (red skin)  
Adjust clothing level

**How can we adapt when we  
are too hot or too cold?**

*Define “thermal  
comfort”*

# Thermal Comfort - Definitions

**Definition 1:** Conditions wherein the average person does not experience the feeling of discomfort (Olgay).

**Definition 2:** A condition of mind which expresses satisfaction with the thermal environment as assessed by subjective evaluation (ASHRAE 55 - 2004).

# ASHRAE 7-point scale



Outdoor Thermal Comfort Study

(Photo courtesy of Jianxiang Huang. Used with permission.)

+3 *Very Hot*

+2 *Hot* *Comfort Range*

+1 *Warm*

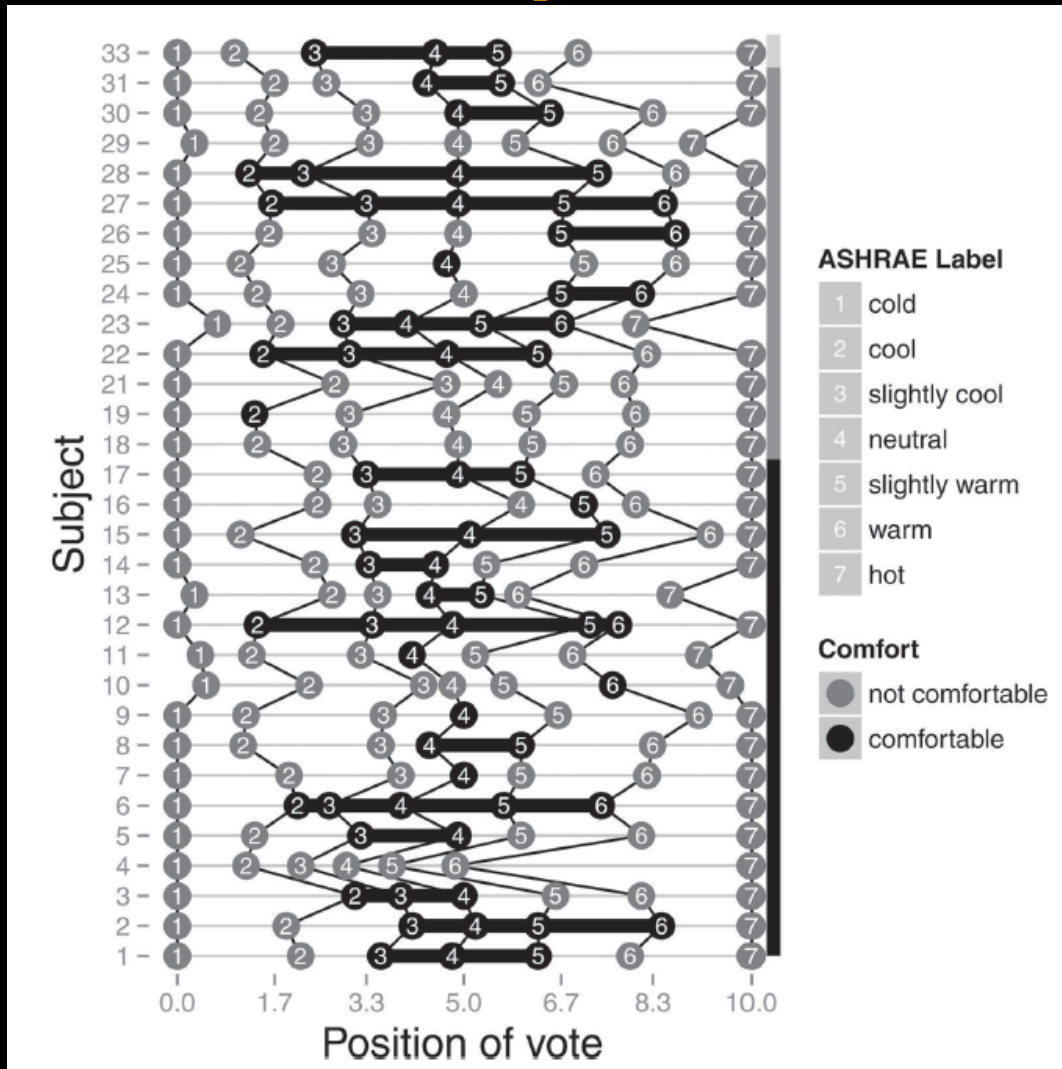
0 *Neutral*

-1 *Cool*

-2 *Cold*

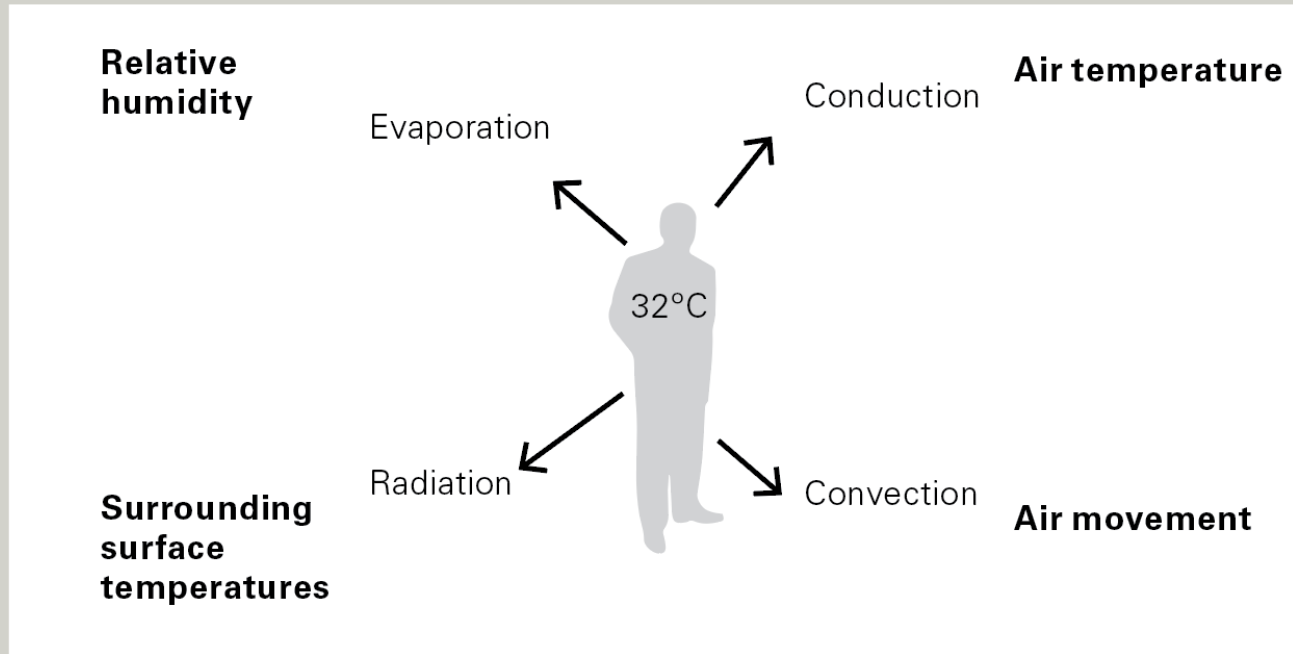
-3 *Very Cold*

# ASHRAE 7-point scale



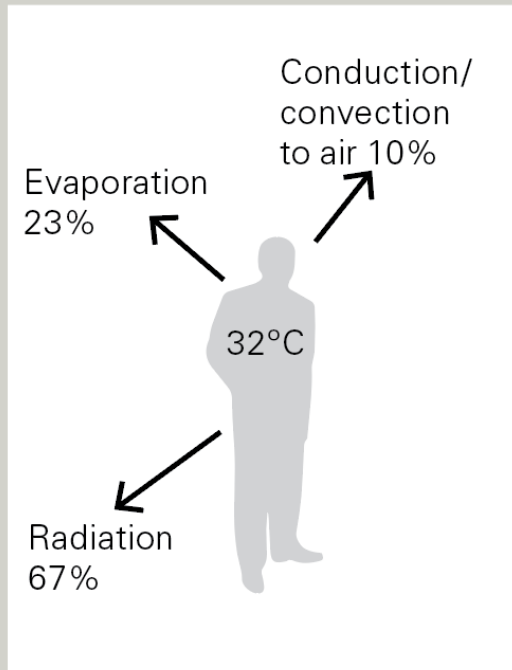
Source: M Schweiker, X Fuchs, S Becker, M Shukuya, M Dovjak, M Hawighorst and J Kolarik, "Challenging the assumptions for thermal sensation scales," *Building Research and information*, 45:5, pp. 572-589, 2016. © Schweiker et al. All rights reserved. This content is excluded from our Creative Commons license. For more information, see <https://ocw.mit.edu/help/faq-fair-use/>.

# What variables are influencing thermal comfort?

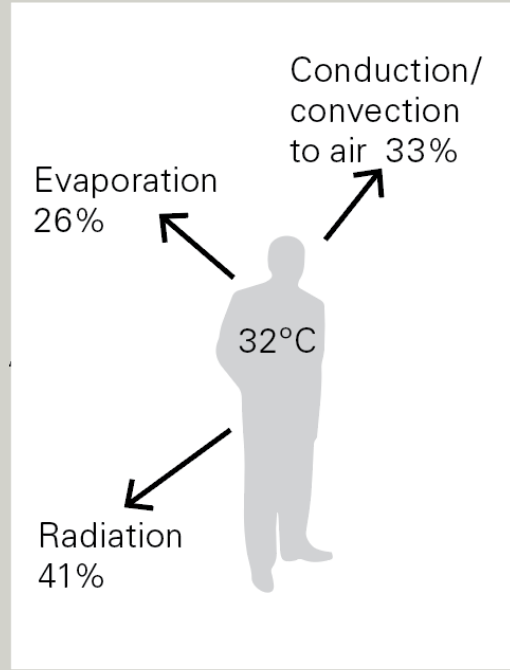


Personal factors: Clothing and activity

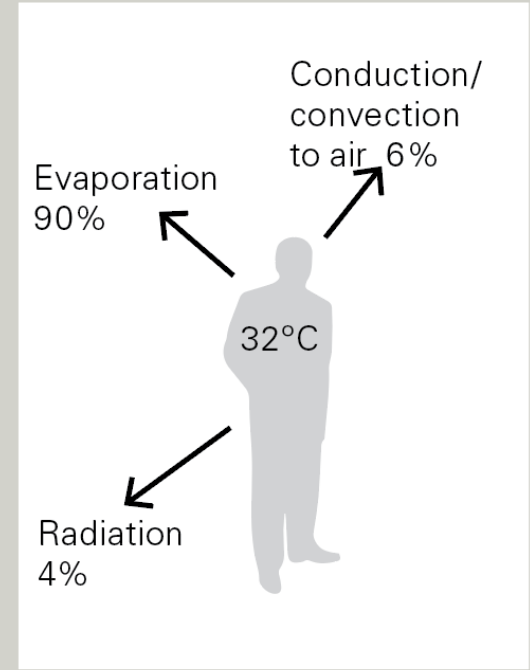
# How do we regulate our body temperature?



Air 24°C



Air 30°C



Air 35°C

# Comfort Range

Depends on individuals' metabolism, clothing and activity level, season, and to a smaller degree on food and drink intake, body shape, age, and gender.

Relative humidity:

30% to 65%	little effect
<30%	dry skin and mucous membranes
>65%	restricted evaporation

Air velocity:

<0.1 m/s	stuffy
0.2 to 0.5	pleasant
0.5 to 1	awareness
1 to 1.5	drafty



# Metabolic Rates

The metabolic rate, or human body heat production, is often measured in the unit "Met". The metabolic rate of a relaxed seated person is 1 Met, where 1 Met = 58 W/m<sup>2</sup>.

Activity	W/m <sup>2</sup>	W*	Btu/hr	Met
Seated relaxed	58	104	356	1.0
Standing relaxed	70	126	430	1.2
Standing, light activity	93	167	571	1.6
Walking on the level, 2 km/h	110	198	675	1.9
Walking on the level, 5 km/h	200	360	1228	3.4
Sports - Running in 15 km/h	550	990	3377	9.5

Source: ASHRAE 55 – 2004 (page 15).

Metabolic rates are given in W per area of skin. A “typical” adult has an effective skin surface area of 1.8 m<sup>2</sup>. => 1 person radiates about 100 W (an incandescent light bulb).

# Clothing

TABLE B1  
Clothing Insulation Values for Typical Ensembles<sup>a</sup>

Clothing Description	Garments Included <sup>b</sup>	$I_{cl}$ (clo)
Trousers	1) Trousers, short-sleeve shirt	0.57
	2) Trousers, long-sleeve shirt	0.61
	3) #2 plus suit jacket	0.96

Source: ASHRAE 55 – 2004 (page 15)

# Thermal Comfort Index

Thermal comfort indices are assessment methods of thermal sensation and comfort. More than 100 thermal comfort indices have been developed over the last 100 years.

**Actual Sensation Vote** (Nikolopoulou, 2004); **Adaptive Thermal Index** (Humphrey, 1975); **Apparent Temperature** (Steadman, 1979); **Discomfort Index** (Thom, 1959); **Effective Temperature Scale** (Houghton et al. 1923); **ETU** (Nagano & Horikoshi, 2011); **ETF** (Kurazumi et al., 2010); **Humid Operative Temperature** (Horikoshi et al., 1991); **Local SET** (Kohri and Mochida, 2003); **New Effective Temperature ET\*** (Gagge et al. 1971) **Outdoor Standard Effective Temperature** (Spagnolo and de Dear 2003); **Perceived Temperature** (Tinz and Jendritzky 2003); **Perceived Temperature** (Staiger, et al, 2011); **Physiologically Equivalent Temperature** (Höppe 1999); **Predicted Mean Vote, Predicted Percentage Dissatisfied** (Fanger, 1972); **Standard Effective Temperature** (Gagge et al. 1986); **Seven-Point Thermal Comfort Scale** (Bedford, 1936); **Temperature-Humidity Index** (Clarke & Bach, 1971) **UTCI** (ISO, 2009); **Thermal Comfort Zone** (Houghton & Yaglou, 1923) **Wind Chill Index** (Steadman, 1971); **Wind Chill Temperature Index** (OFCM, 2003);

# Predicted Mean Vote

$$(0.352 * \exp(-0.042 * M/A_{Du}) + 0.032) * \{ M/A_{Du} * (1 - \eta) - 0.35$$

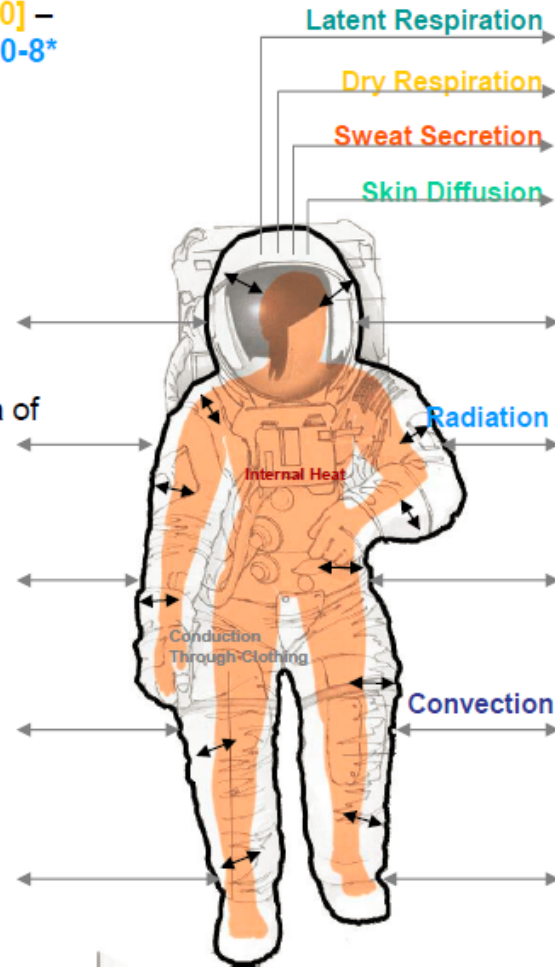
$$[43 - 0.061 * M/A_{Du} * (1 - \eta) - p_a] - 0.42 [M/A_{Du} * (1 - \eta) - 50] -$$

$$0.0023 M/A_{Du} * (44 - p_a) - 0.0014 * M/A_{Du} * (34 - t_a) - 3.4 * 10^{-8} *$$

$$f_{cl} [(t_{cl} + 273)^4 - (t_{mrt} + 273)^4] - f_{cl} * h_c * (t_{cl} - t_a) \}$$

- M** Metabolism rate (kcal/ hr )
- A<sub>Du</sub>** Surface area of the nude body (m<sup>2</sup>)
- η** W/M body movement work / heat ratio
- p<sub>a</sub>** Water vapor pressure (mmHg)
- f<sub>cl</sub>** Ratio of surface area of the clothed body to the surface area of nude body
- I<sub>cl</sub>** Thermal resistance of the clothing (0 ~ 1)
- t<sub>a</sub>** Air temperature °C
- t<sub>mrt</sub>** Mean radiant temperature °C
- t<sub>cl</sub>** Temperature of clothes external surface °C
- $$t_{cl} = 35.7 - 0.032 * M / A_{Du} * (1 - \eta) - 0.18 I_{cl} * [3.4 * 10^{-8} (-8) * f_{cl} * [(t_{cl} + 273)^4 - (t_{mrt} + 273)^4] + f_{cl} * h_c * (t_{cl} - t_a)]$$
- h<sub>c</sub>** Heat transfer coefficient forced convection
- $$h_c = 2.05 * (t_{cl} - t_a)^{0.25} \quad \text{if } 2.05 * (t_{cl} - t_a)^{0.25} > 10.4 * V^{0.5}$$
- $$h_c = 10.4 * V^{0.5} \quad \text{if } 2.05 * (t_{cl} - t_a)^{0.25} < 10.4 * V^{0.5}$$
- V** Relative wind speed

(Fanger, 1970)



Ole Fanger wanted to predict conditions for which the largest possible percentage of a given group experiences thermal comfort.

# Predicted Mean Vote

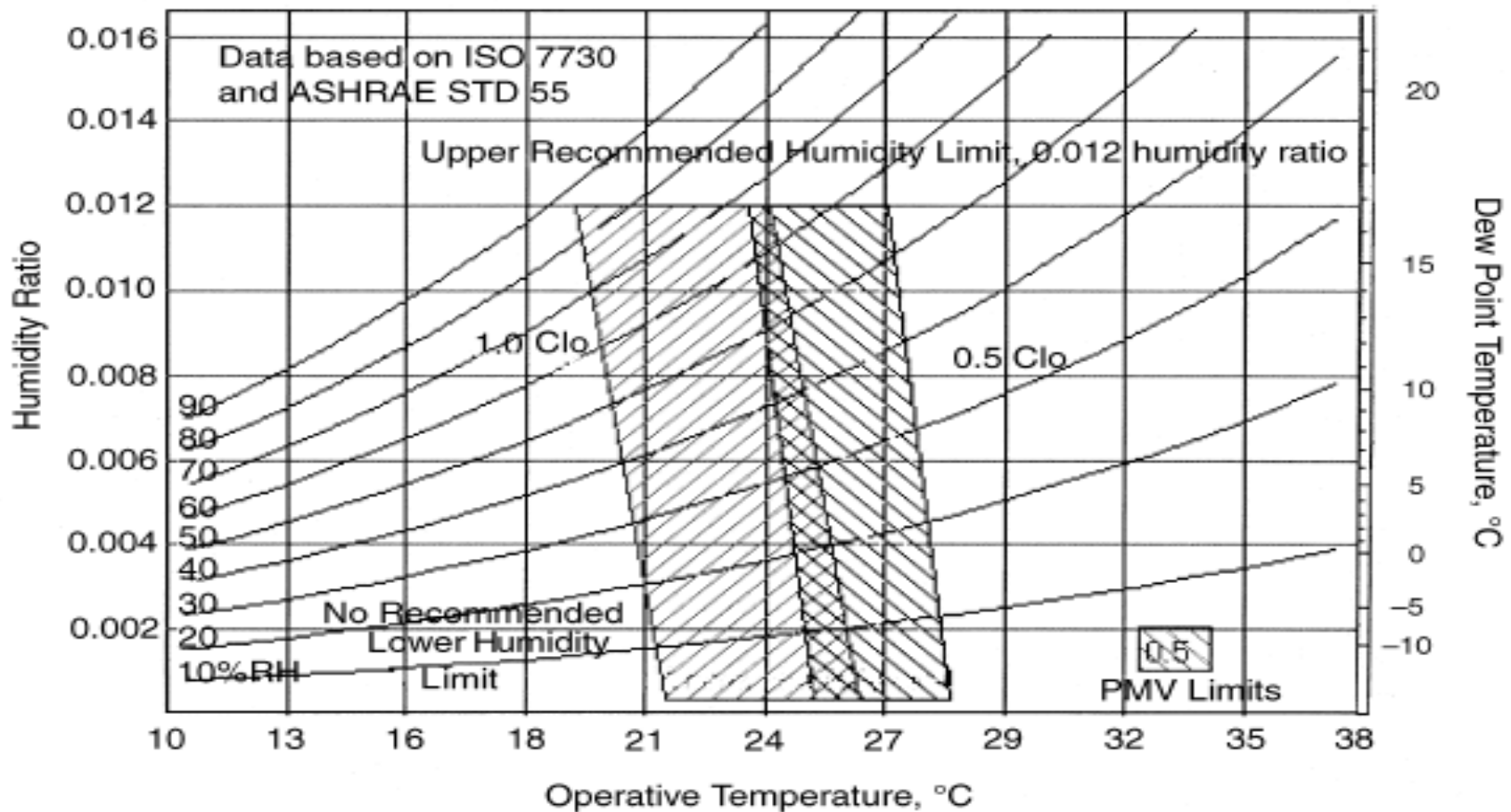
According to Fanger, requirements for steady-state thermal comfort are:

- body is in heat balance
- mean skin temperature and sweat rate are within limits
- no local discomfort exists

PMV is based on experiments with Danish college students exposed to steady-state conditions for 3 hours in a climate chamber.

# ASHRAE Comfort Range

Source: ASHRAE 55 – 2004 (page 5). © ASHRAE. All rights reserved. This content is excluded from our Creative Commons license. For more information, see <https://ocw.mit.edu/help/faq-fair-use/>.



□ Note, the X-axis is provided in operative instead of dry bulb temperature.

□ Figure applies for a metabolic rate of 1.0 to 1.3 met and a clothing level of 0.5 to 1.0 clo, air speed <0.2 m/s.

# ASHRAE 55

Compliance with PMV is required in air conditioned spaces.

# CBE Thermal Comfort Tool

ASHRAE-55

EN-15251

Compare

Ranges

Upload

Select method:

PMV method

Air temperature

25 °C

Use operative temperature

Mean radiant temperature

25 °C

Air speed

0.1 m/s

Local air speed control

Humidity

50 %

Relative humidity

Metabolic rate

1.1 met

Typing: 1.1

Clothing level

0.5 clo

Typical summer indoor

Create custom ensemble

Dynamic predictive clothing

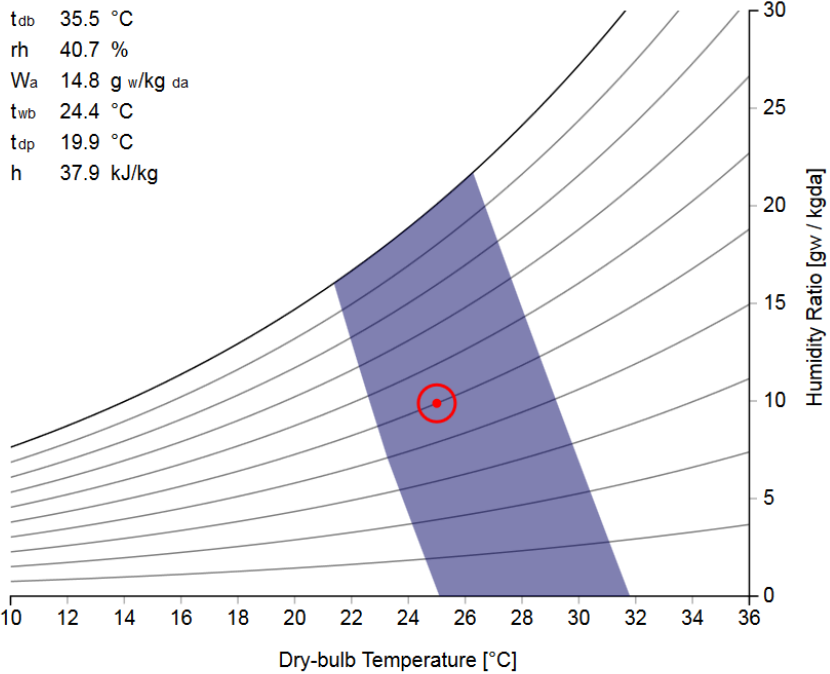
LEED documentation

Globe temp SolarCal Specify pressure SI IP Local discomfort ? Help

✓ Complies with ASHRAE Standard 55-2013

PMV -0.13  
 PPD 5%  
 Sensation Neutral  
 SET 24.5°C

Psychrometric chart (air temperature)



<http://comfort.cbe.berkeley.edu/>

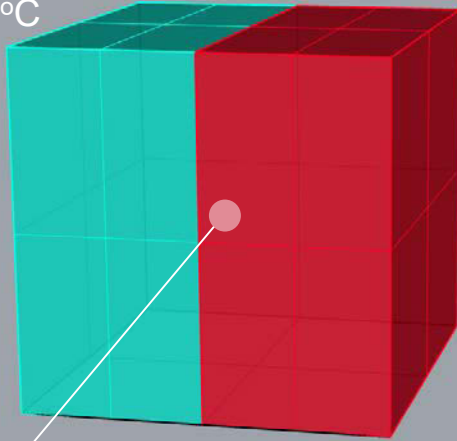


# Mean Radiative Temperature [MRT]

The uniform surface temperature of an imaginary black enclosure in which an occupant would exchange the same amount of radiant heat as in the actual non uniform space. Source: ASHRAE 55

**Non-uniform space**

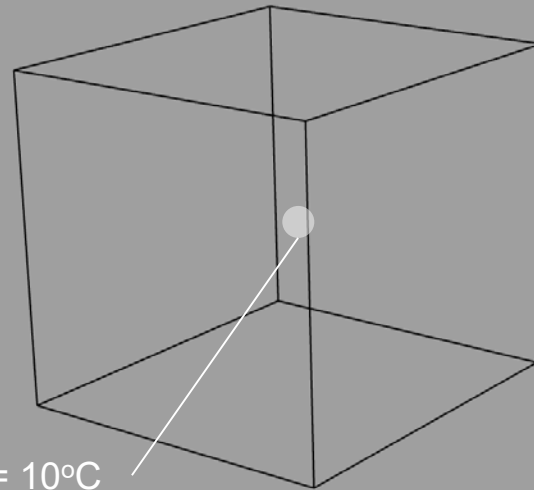
$T_{\text{surfaces blue}} = 0^{\circ}\text{C}$   
 $T_{\text{surfaces red}} = 20^{\circ}\text{C}$



$T_{\text{MRT}} = 10^{\circ}\text{C}$

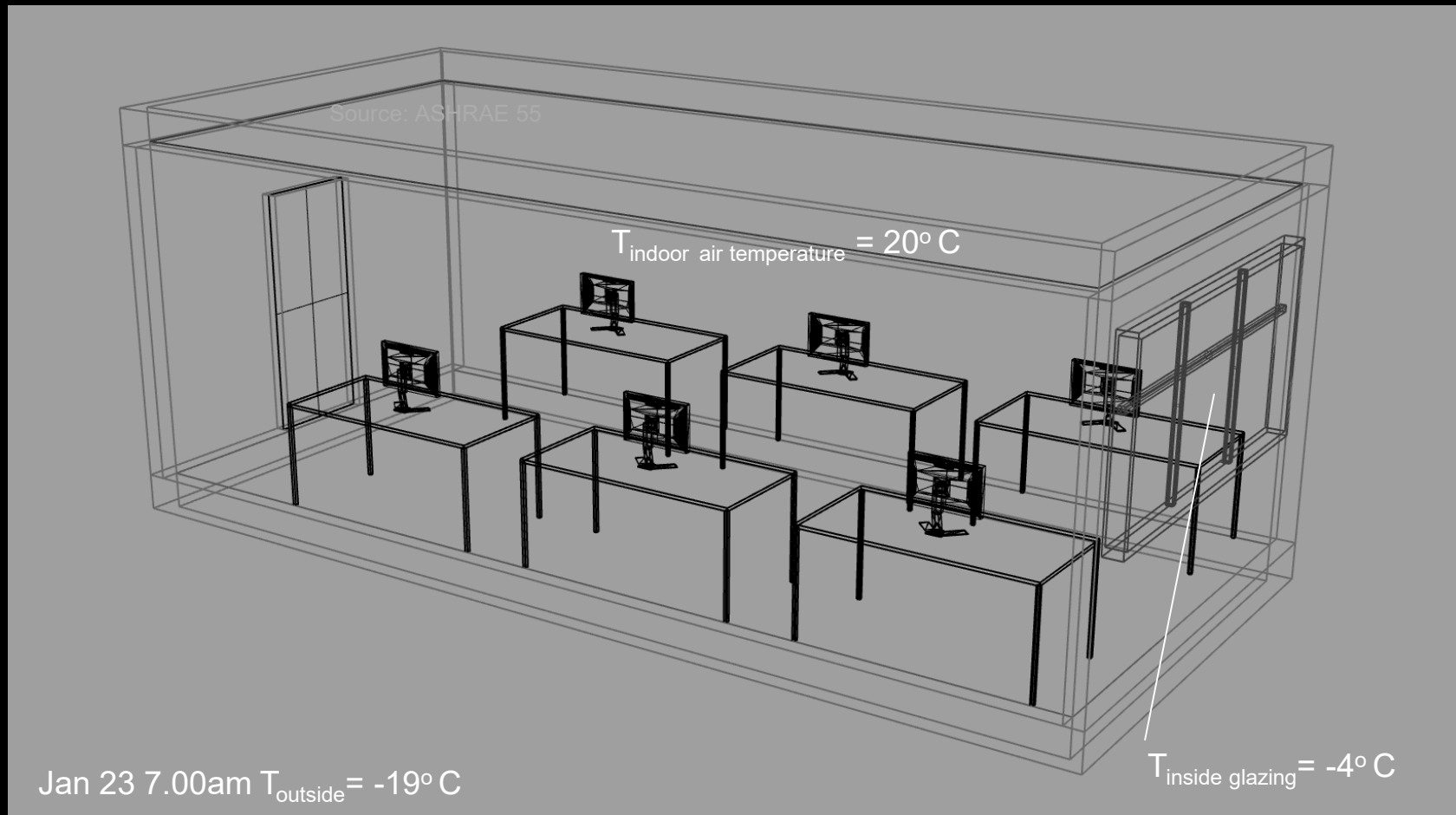
**Uniform space**

$T_{\text{surfaces grey}} = 10^{\circ}\text{C}$



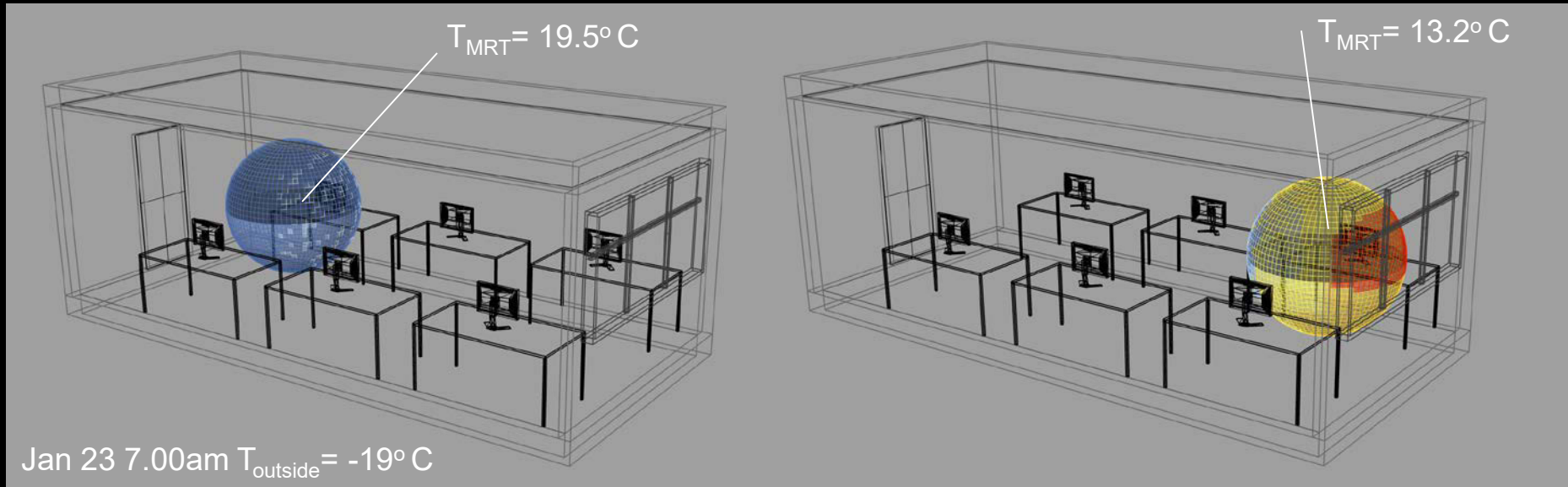
$T_{\text{MRT}} = 10^{\circ}\text{C}$

# Mean Radiative Temperature Field



- ❑ The reference office is heated to  $20^{\circ}\text{C}$ .
- ❑ The surface of the single pane window is colder ( $-4^{\circ}\text{C}$ ) than the surfaces of the floor, ceiling and walls.

# Mean Radiative Temperature Distribution



- ❑ The mean radiant temperature throughout the space depends on the exposure of a given point to the different surrounding surfaces.
- ❑ Even with an ideal forced-air heating/cooling system somebody sitting near the single pane window might get cold/hot.

*How large is this effect over the course of the year?*

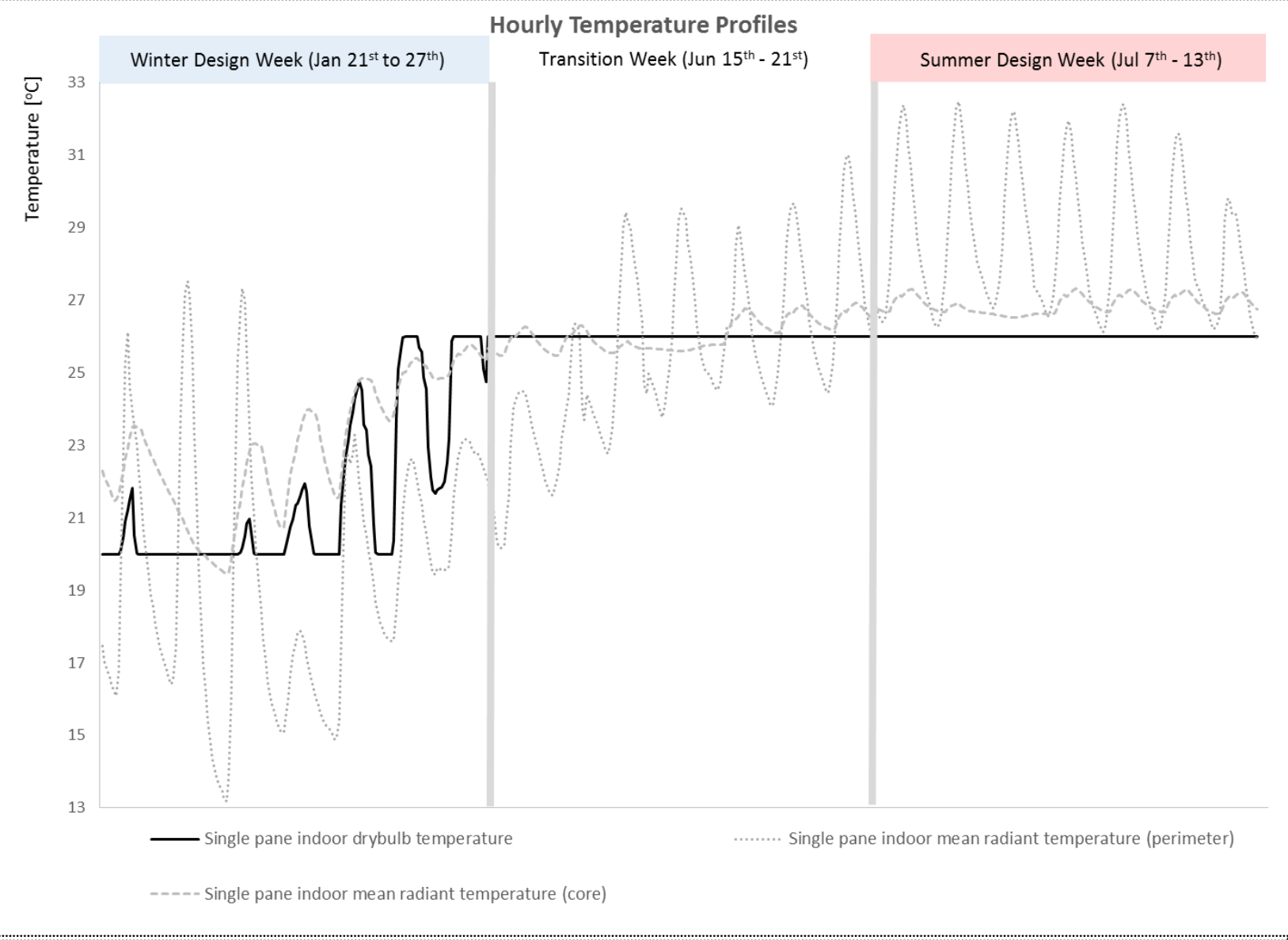
# Winter/Summer Design Week

**Winter design week** - a week identified by the weather data translator as being the coldest of the year.

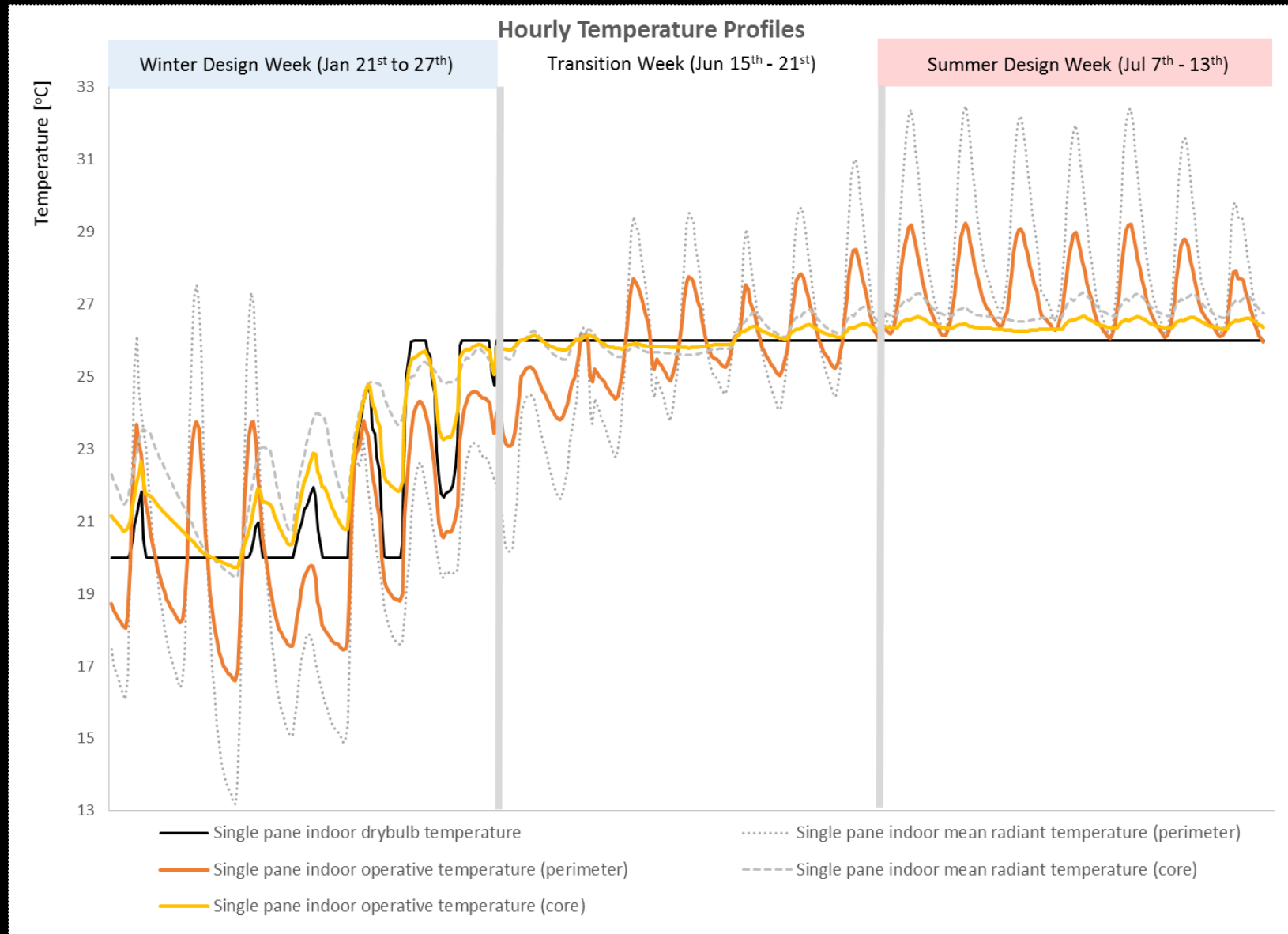
**Summer design week** - a week identified by the weather data translator as being the hottest of the year.

**Transition period** - a typical week between the heating and cooling periods.

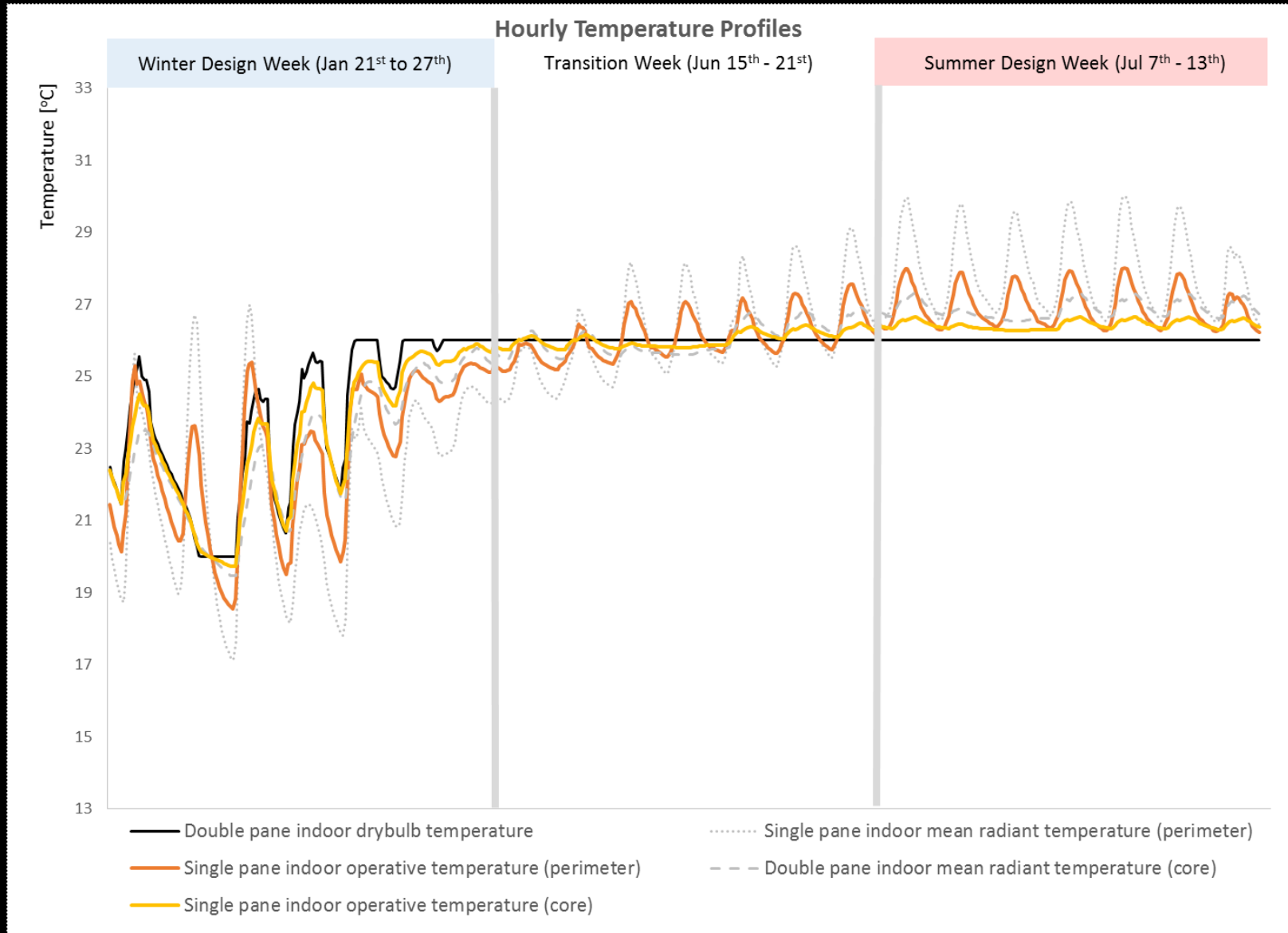
# Conditioned Office with Single Pane Window



# Conditioned Office with Single Pane Window



# Conditioned Office with Double Pane Window





# Measuring Radiative Temperature



# Mean Radiative Temperature Calculation

To measure the mean radiant temperature at a particular reference point,  $x$ , you can use a spot thermometer to measure the surface temperature of all surfaces “seen” from  $x$ . You also need to estimate the Form Factor (FF) of each surface with respect to  $x$ . A form factor is the fraction of the solid angle that a given surface takes within the point of view of a point to the full solid angle ( $2\pi$ ) surrounding the point. The sum of all form factors is 1.

$$MRT^4 = \text{Form\_Factor}_1 \times MRT_1^4 + \text{Form\_Factor}_2 \times MRT_2^4 \dots$$

with  $MRT_i$  = temperature of surface  $i$  in Kelvin;  $FF_i$  = form factor of surface  $i$

For the space below all surfaces except for the screen had a temperature of 26°C. The screen had a temperature of 43°C. Assuming that the screen takes up an estimated 7% of the surrounding surfaces from the position of a person seated at the desk, the MTR (in Kelvin) becomes:

$$MRT^4 = 0.93 \times (273 + 26) K^4 + 0.07 \times (273 + 43) K^4 \Rightarrow MRT = 300.3 K = 27.3 \text{ } ^\circ\text{C}$$



# Operative Temperature

The operative temperature approximates how one “feels” in a given thermal environment.

$$\text{Operative Temperature} \sim 0.5 * \text{MRT} + 0.5 * \text{DBT}$$

# Thermal Stress

## Rule of Thumb

To maintain thermal comfort the difference between the MRT and DBT in a space should be no more than 3-4 K. For specific surfaces ASHRAE 55 allows for the following asymmetries for different surfaces:

**TABLE 5.2.4.1**  
**Allowable Radiant Temperature Asymmetry**

Radiant Temperature Asymmetry °C (°F)			
Warm Ceiling	Cool Wall	Cool Ceiling	Warm Wall
< 5 (9.0)	< 10 (18.0)	< 14 (25.2)	< 23 (41.4)

Source: ASHRAE 55 – 2004 (page 7)

*Can we do better?*

# Thermal Neutrality vs. Preferred Thermal Sensation

Photo courtesy of [Pat Dye](#) on Flickr. License CC BY-NC-SA.



Nobody on this photo is comfortable according to Thermal Comfort Indices.

Thermal neutrality is boring.

Thermal neutrality is influenced by season.

Individuals in air conditioned buildings are twice as sensitive as occupants of naturally ventilated buildings.

<https://mitpress.mit.edu/books/thermal-delight-architecture>

# ASHRAE 55

Accepted temperature range depends on whether a space is 'conditioned' or not.

Two compliance paths:

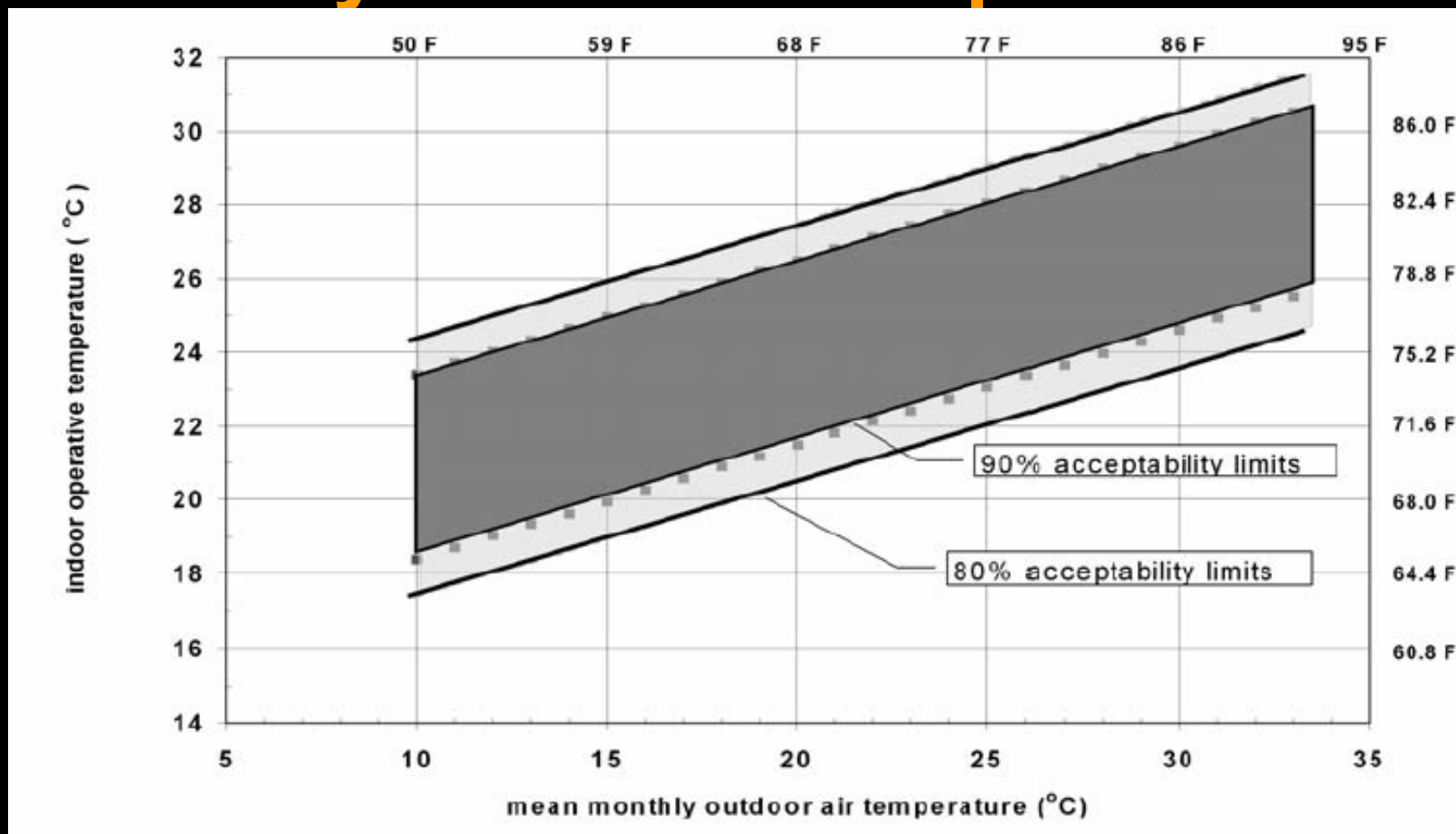
- Predictive Mean Vote
- Adaptive Temperature



# Mean Monthly Outdoor Temperature

Arithmetic average of the mean daily minimum and mean daily maximum outdoor (dry-bulb) temperatures for the month in question (ASHRAE 55).

# Acceptable operative temperature in naturally conditioned spaces



Source: ASHRAE 55 – 2004 (page 10)

Clothing level is assumed to vary 'naturally' with season. No humidity or air speed limits. Comment: Clarified legal implications for 'naturally conditioned' spaces in the US.

# CBE Thermal Comfort Tool

ASHRAE-55

EN-15251

Compare

Ranges

Upload

Select method:

Adaptive method

Air temperature

18 °C

Use operative temperature

Mean radiant temperature

20 °C

Prevailing mean outdoor temperature

29 °C

Air speed

0.3 m/s (59 fpm)

LEED documentation

Globe temp

SolarCal

Specify pressure

SI IP

Local discomfort

? Help

**X Does not comply with ASHRAE Standard 55-2013**

80% acceptability limits

↳ Status

Operative temperature: 23.3 to 30.3°C

Too warm

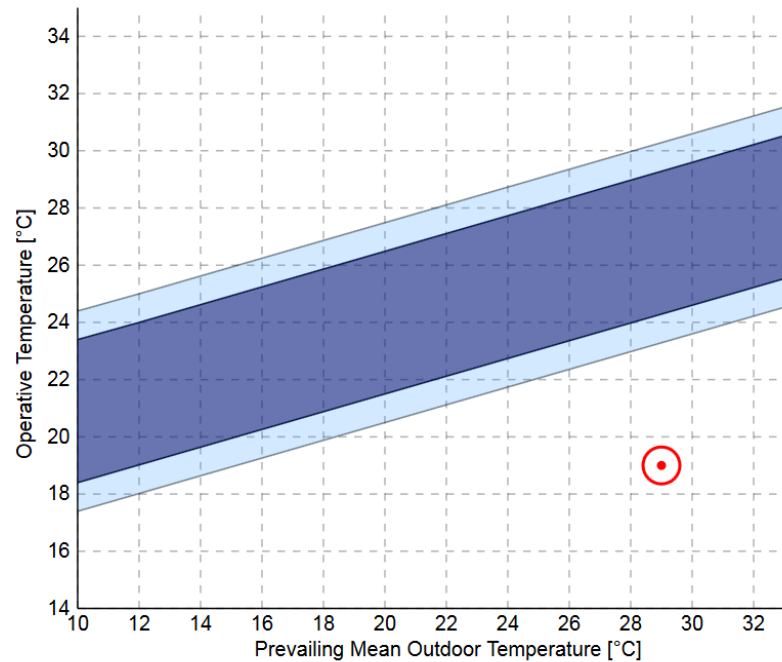
90% acceptability limits

↳ Status

Operative temperature: 24.3 to 29.3°C

Too warm

Adaptive chart



<http://comfort.cbe.berkeley.edu/>

# Critique of Thermal Comfort Models

## ❑ Hypothesis has not been demonstrated

How will an average person feel? = How will a large group respond?

## ❑ Model variation too large

- group variance = 1.0 scale units
- inter-individual variance = 1.0 scale unit
- intra-individual variance 1.0 scale unit (season, mood, alertness)

## ❑ Model weak at the extremes of comfort

## ❑ Cultural differences

- Thermal neutrality in Malaysia and London varies by 3 K

# 'Enforcement' of ASHRAE 55

- Declare exceedances such as 1% of time, 29 hours per year....
- Difficult to meet with large architectural glazings.
- Extra Credit under LEED.

# Lessons for design

- ❑ Provide building occupants with thermal control over their environment (thermostats, fans, blinds, operable windows...).
- ❑ Allow occupants to dress as desired.

# Questions?

MIT OpenCourseWare  
<https://ocw.mit.edu/>

4.401/4.464 Environmental Technologies in Buildings Fall 2018

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