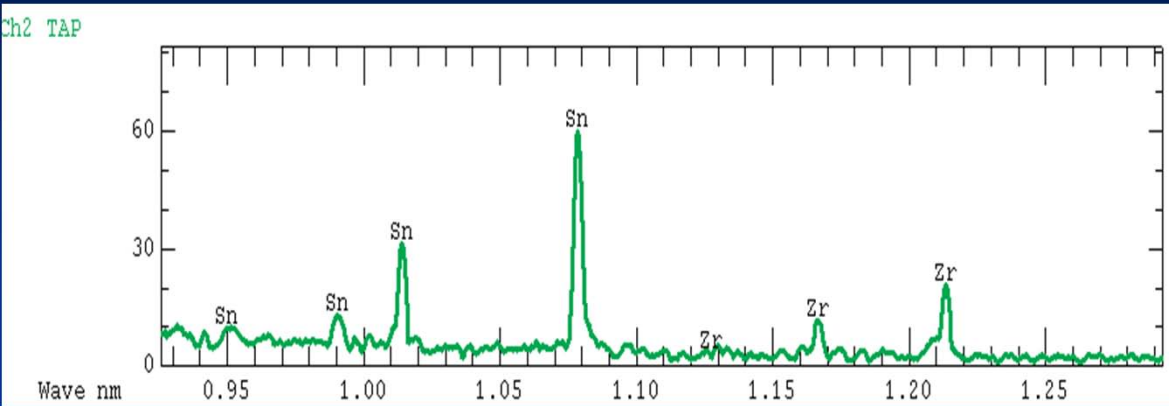


EPMA: Quantitative analysis



*WDS spectrum:
Intensity is proportional
to concentration*

$$\frac{C_i}{C_{(i)}} \propto \frac{I_i}{I_{(i)}} \quad \text{where,} \quad \frac{I_i}{I_{(i)}} = k_i$$

$$\frac{C_i}{C_{(i)}} = k_i \cdot [\mathbf{ZAF}]_i$$

C_i and $C_{(i)}$: concentration of element 'i' in sample and standard

I_i and $I_{(i)}$: measured X-ray intensities of element 'i' in sample and standard

k_i : k-ratio of element 'i'

ZAF : matrix corrections

Matrix (ZAF) corrections

Z : *atomic number correction*

A : *absorption correction*

F : *fluorescence correction*

Atomic number (Z) correction

$$\mathbf{Z}_i \approx \frac{\frac{R_i}{S_i}}{\frac{R_i^*}{S_i^*}}$$

* *sample*

$$R = \Sigma C_j R_j$$

[*R = #X-ray photons generated / #photons if there were no back-scatter*]

$$S = \Sigma C_j S_j$$

[*S = $-(1/\rho)(dE/ds)$, stopping power*]

Z, a function of E_0 and composition

Duncumb-Reed-Yakowitz method:

$$R_i = \sum_j C_j R_{ij}$$

$$R_{ij} = R'_1 - R'_2 \ln(R'_3 Z_j + 25)$$

$$R'_1 = 8.73 \times 10^{-3} U^3 - 0.1669 U^2 + 0.9662 U + 0.4523$$

$$R'_2 = 2.703 \times 10^{-3} U^3 - 5.182 \times 10^{-2} U^2 + 0.302 U - 0.1836$$

$$R'_3 = (0.887 U^3 - 3.44 U^2 + 9.33 U - 6.43) / U^3$$

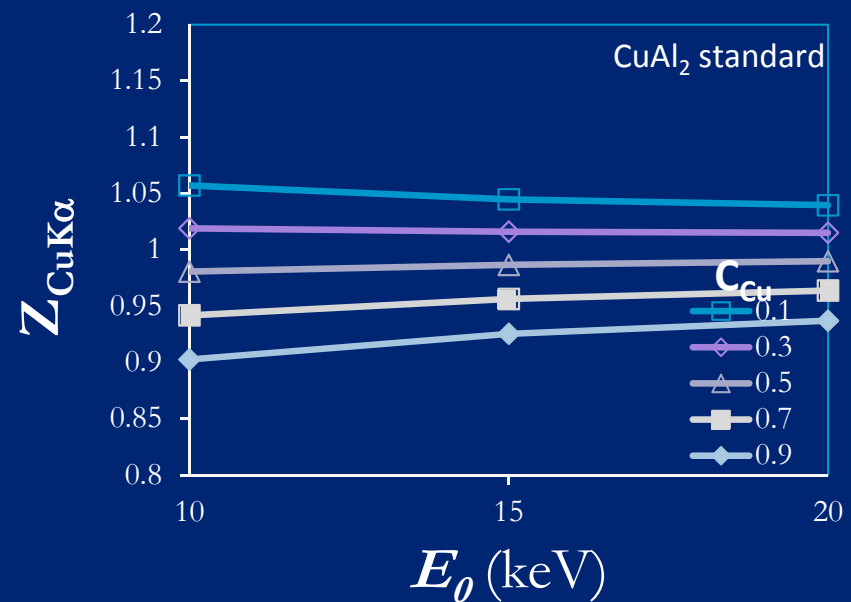
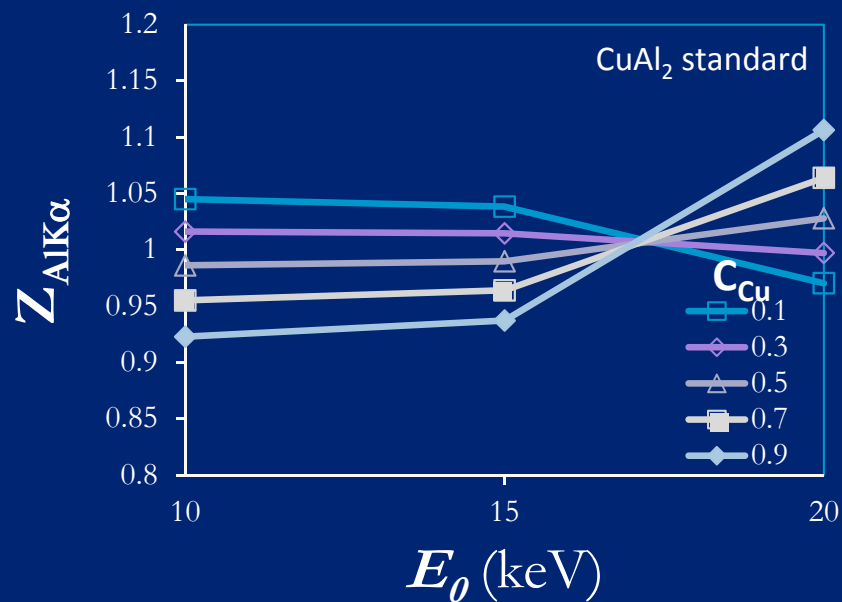
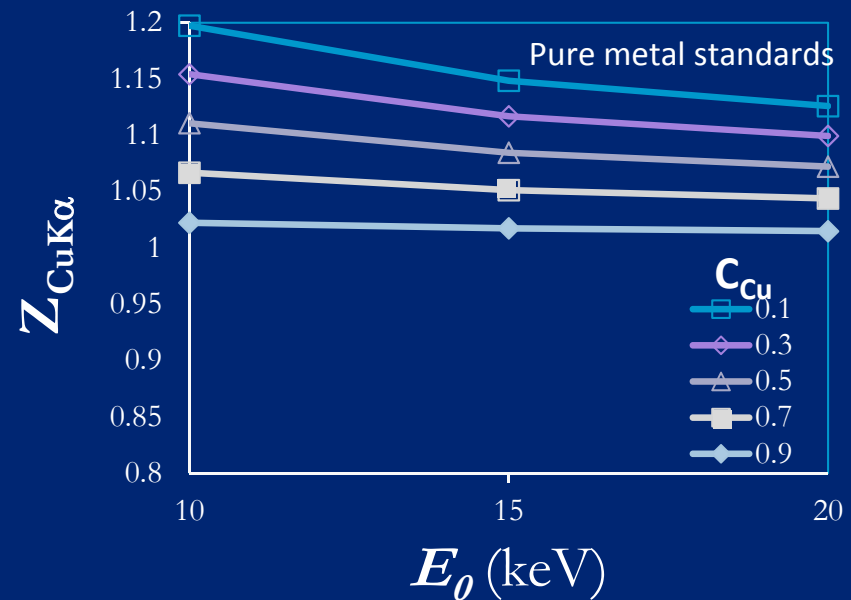
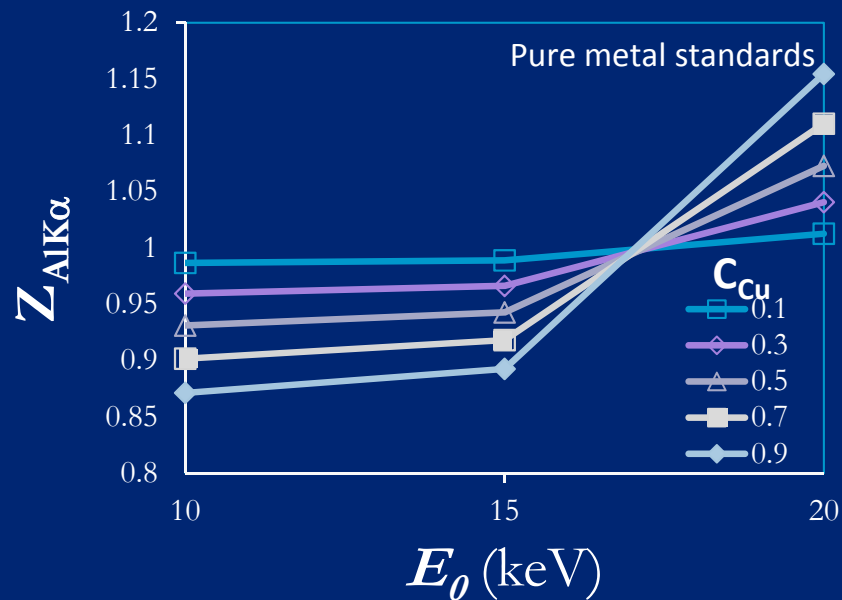
$$S_i = \sum_j C_j S_{ij}$$

$$S_{ij} = (\text{const}) [(2Z_j/A_j)/(E_0 + E_c)] \ln[583(E_0 + E_c)/J_j]$$

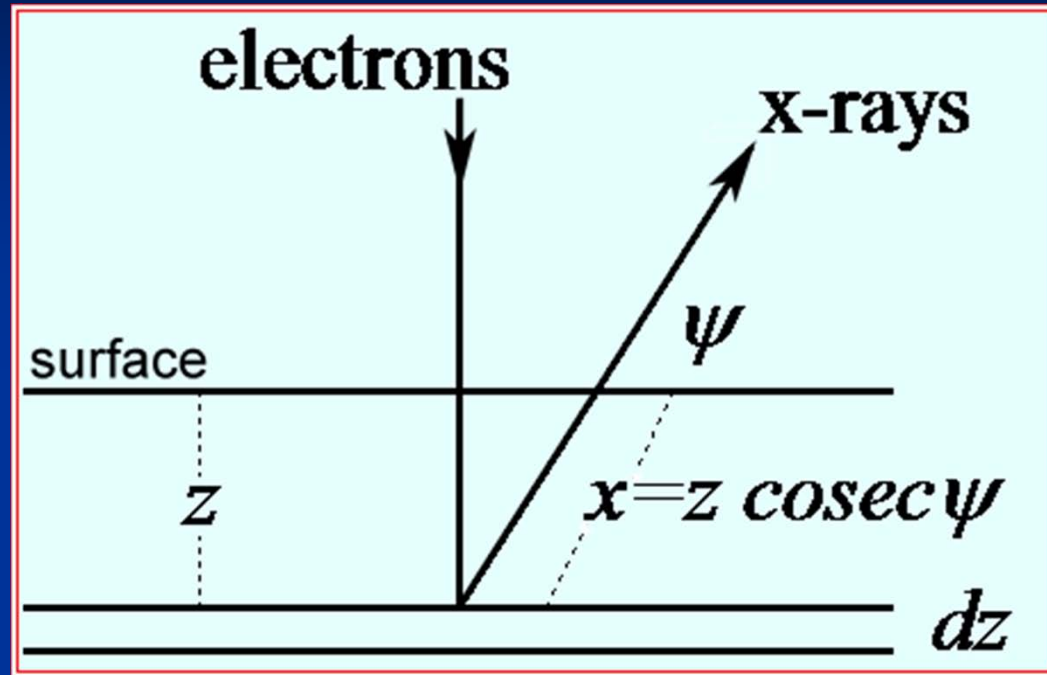
$$\text{where, } J \text{ (keV)} = (9.76Z + 58.82Z^{0.19}) \times 10^{-3}$$

Z, a function of E_0 and composition

Al-Cu alloy



X-ray absorption



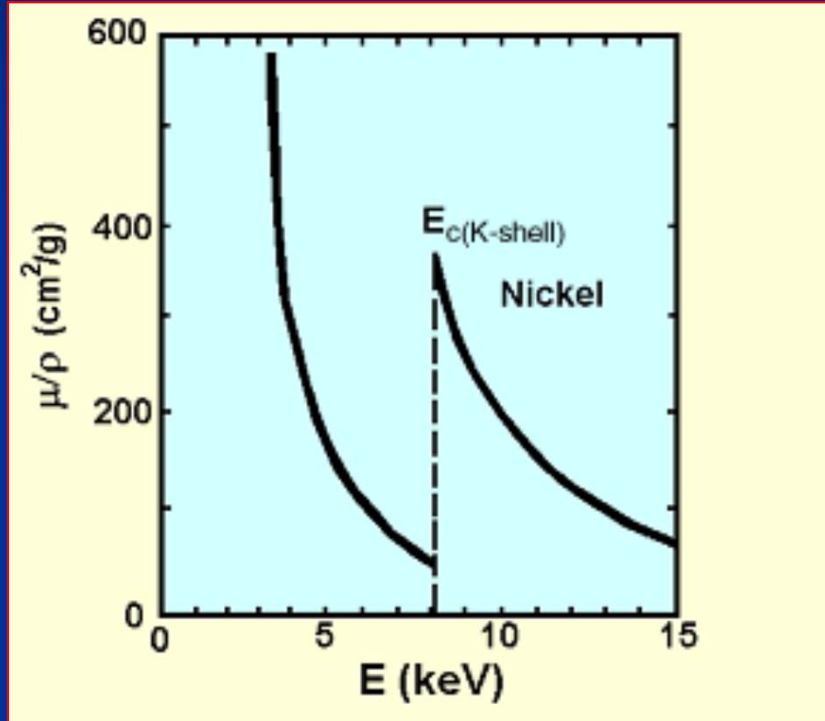
$$I = I_0 \exp^{-(\mu/\rho)(\rho x)} = I_0 \exp^{-(\mu/\rho)(\rho z \operatorname{cosec} \psi)}$$

I : Intensity emitted; I_0 : Intensity generated

μ/ρ : mass absorption coefficient

ρ : density; z : depth; ψ : take-off angle

Mass absorption coefficient, $(\mu/\rho)_{\text{absorber}}^{\text{energy}}$



A function of energy being absorbed

	Energy (keV)	$E_{c(K\ shell)}$ (keV)	$(\mu/\rho)_{Ni}^{\text{energy}}$ (cm ² /g)
CoK α	6.925		53
NiKα	7.472	<u>8.331</u>	60
CuK α	8.041		49
ZnKα	<u>8.632</u>		<u>311</u>

ZnK α is absorbed by Ni

For compounds,

$$\left(\frac{\mu}{\rho}\right)_{\text{compound}}^{\text{energy}} = \sum_j \left(\frac{\mu}{\rho}\right)_{\text{element 'j'}}^{\text{energy}} C_j$$

Absorption (A) correction

$$\mathbf{A}_i = \frac{f(\chi_i)}{f(\chi_i)^*}$$

* *sample*

Absorption function,

$$f(\chi_i) = I_{i(\text{emitted})} / I_{i(\text{generated})}$$

A, a function of E_0 , ψ and composition

Philibert method:

$$f(\chi_i) = \left[\left(1 + \frac{\chi_i}{\sigma_i} \right) \left(1 + \frac{\chi_i}{\sigma_i} \frac{h_i}{1 + h_i} \right) \right]^{-1}$$

where,

$$\chi_i = \left(\frac{\mu}{\rho} \right)_{\text{specimen}}^{i\text{-energy}} \operatorname{cosec} \psi$$

$$h_i = 1.2A_i/Z_i^2$$

$$\sigma_i = 4.5 \times 10^5 / (E_0^{1.65} - E_{i(c)}^{1.65})$$

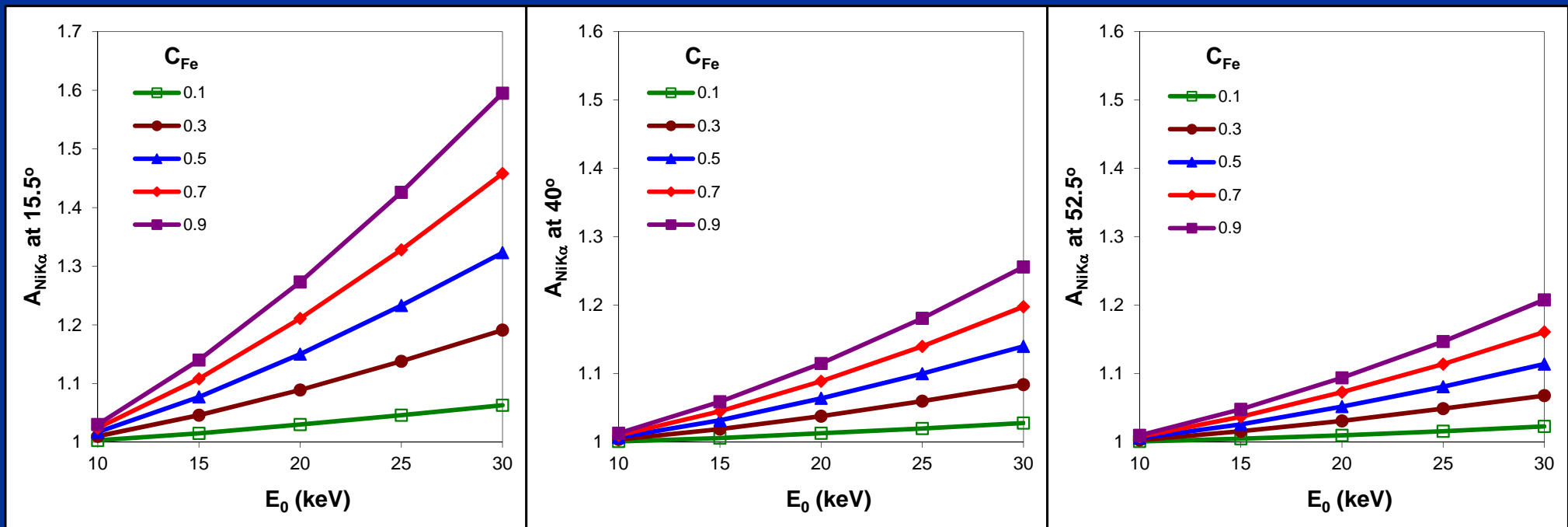
For compounds:

$$h_i = \sum_j h_j C_j$$

$$\left(\frac{\mu}{\rho} \right)_{\text{specimen}}^{i\text{-energy}} = \sum_j \left(\frac{\mu}{\rho} \right)_{\text{element 'j'}}^{i\text{-energy}} C_j$$

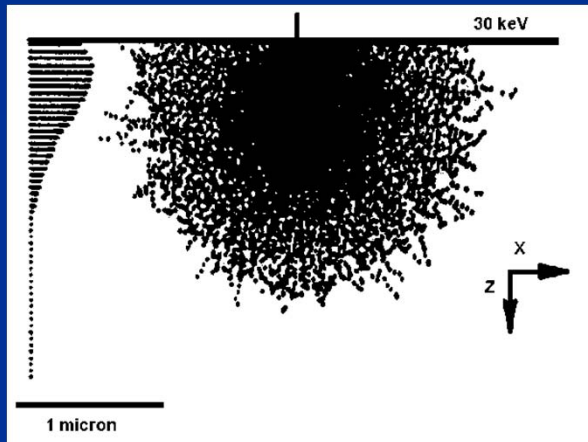
A, a function of E_0 , ψ and composition

$A_{\text{NiK}\alpha}$ in Fe-Ni alloy



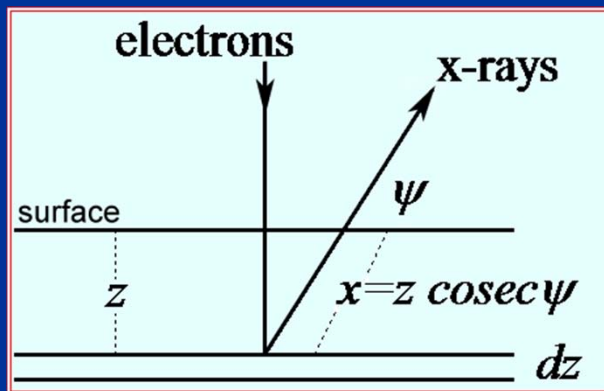
Total X-ray intensity: generated versus emitted

Generated intensity



$$I_{gen} = \phi(\Delta\rho z) \int_0^\infty \phi(\rho z) d(\rho z)$$

Emitted intensity

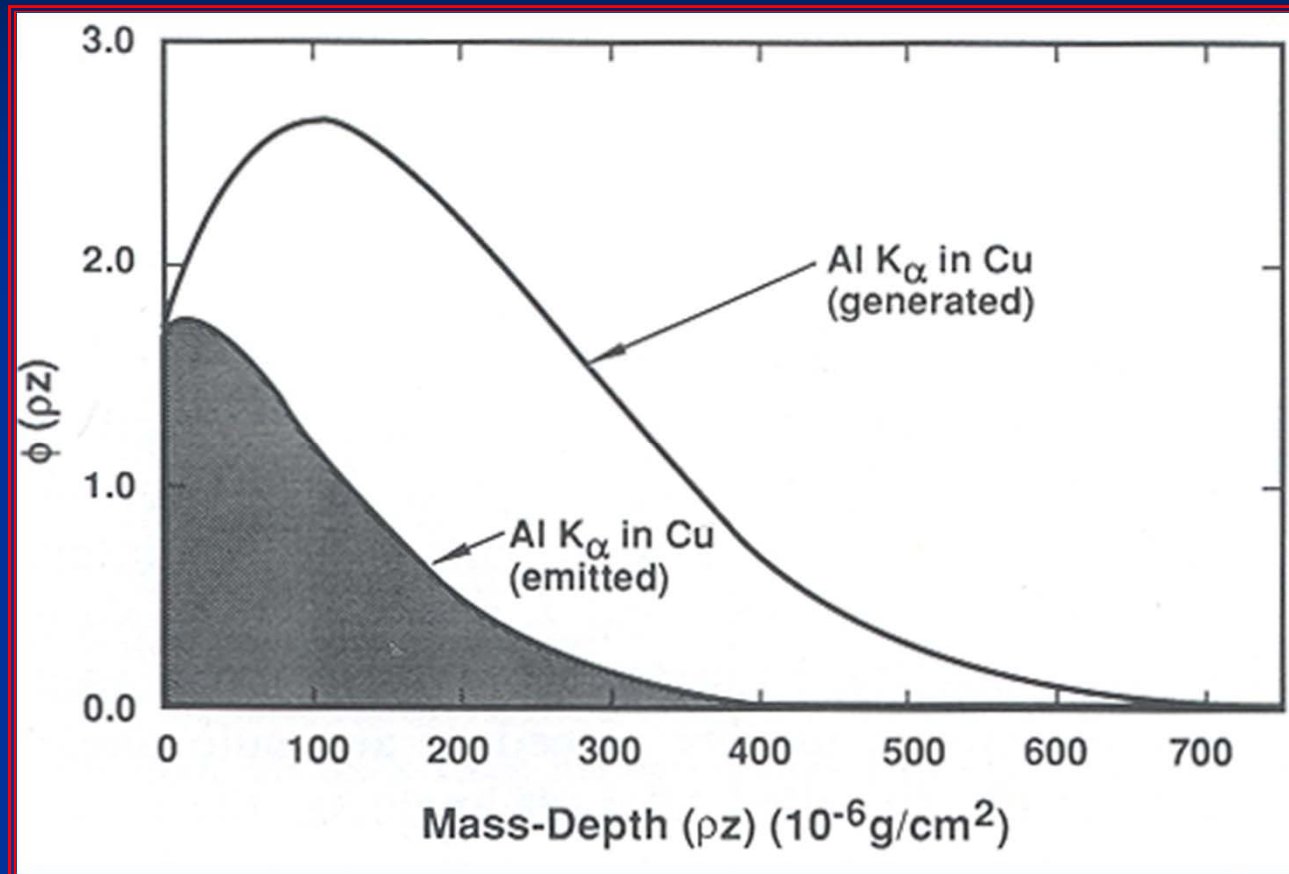


$$I_{emit} = I_{gen} \exp^{-\chi\rho z}$$

$$= \phi(\Delta\rho z) \int_0^\infty \phi(\rho z) \exp^{-\chi\rho z} d(\rho z)$$

where, $\chi = (\mu/\rho) \text{cosec } \psi$

Generated and emitted X-ray intensity variation with depth: AlK α in Al-Cu alloy



Effect of matrix (mainly Cu) on the emitted intensity of AlK α , which is highly absorbed in Cu;

$$\left(\frac{\mu}{\rho}\right)_{\text{Cu}}^{\text{AlK}\alpha} = 4837.5 \text{ cm}^2/\text{g}$$

$\phi(\rho z)$ matrix correction

The combined atomic number and absorption corrections is the ratio of emitted intensities in standard (I_{emit}) to sample (I_{emit}^*)

$$I_{emit} = \phi(\Delta\rho z) \int_0^\infty \phi(\rho z) \exp^{-\chi\rho z} d(\rho z)$$

$$I_{emit}^* = \phi(\Delta\rho z) \int_0^\infty \phi^*(\rho z) \exp^{-\chi\rho z} d(\rho z)$$

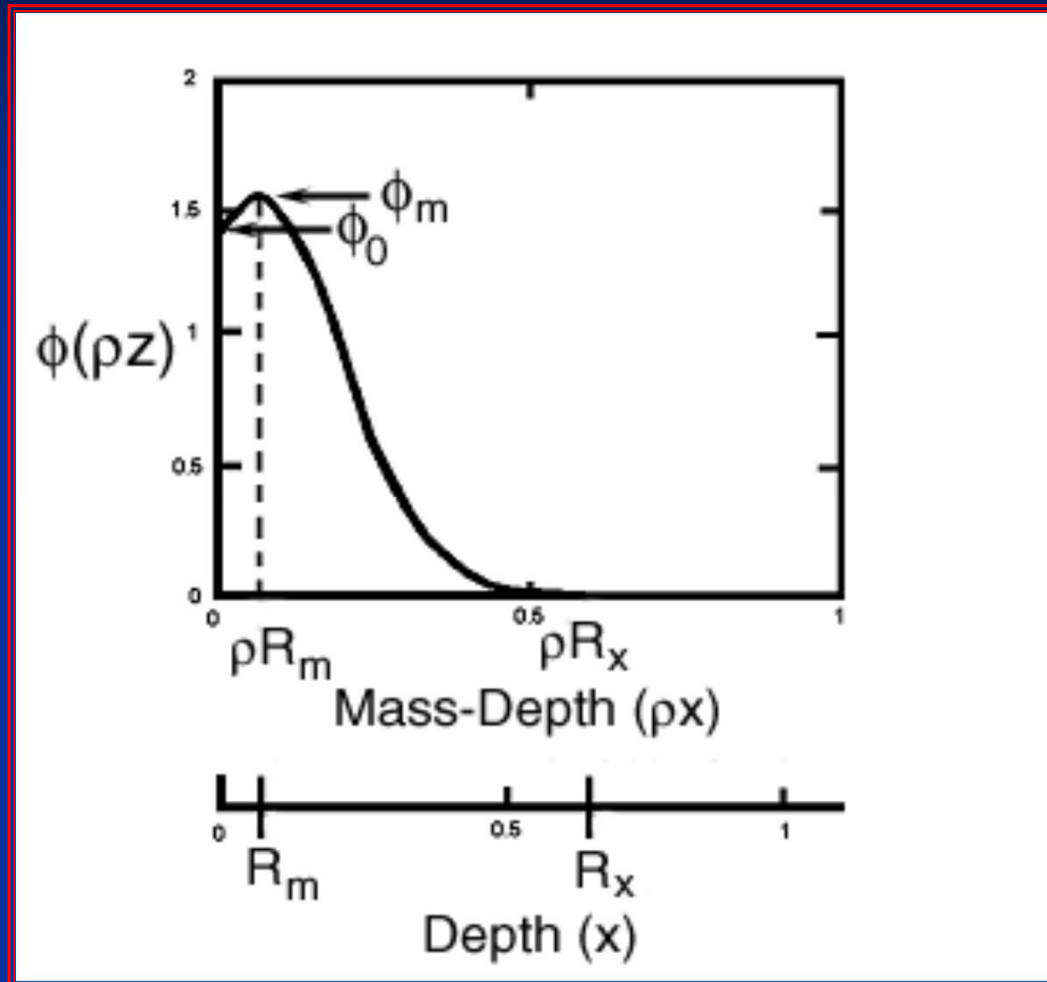
$$\mathbf{Z}_i \mathbf{A}_i = \frac{\int_0^\infty \phi_i(\rho z) \exp^{-\chi_i \rho z} d(\rho z)}{\int_0^\infty \phi_i^*(\rho z) \exp^{-\chi_i \rho z} d(\rho z)}$$

$\phi(\rho z)$ matrix correction

ϕ_0 : the value of $\phi(\rho z)$ at $\rho z=0$

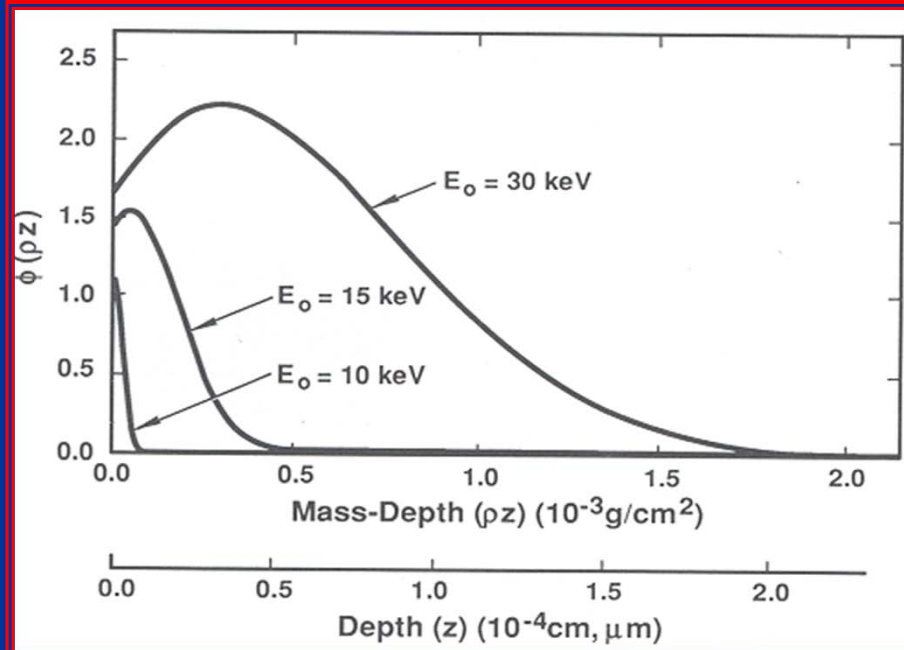
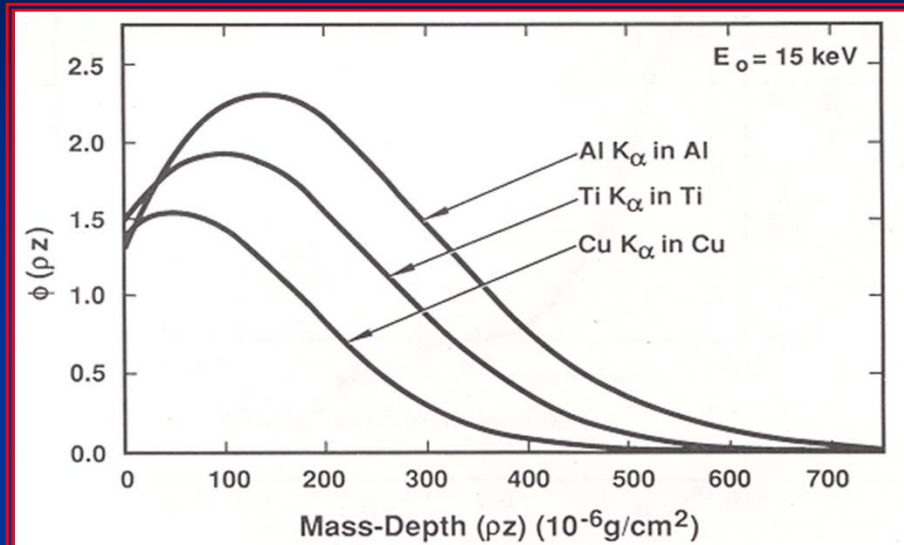
R_m : the depth at which $\phi(\rho z)$ is maximum (ϕ_m)

R_x : the maximum depth of X-ray production (X-ray range)



$Z_i A_i$ is modeled in terms of ϕ_0 , R_m , R_x and the integral of the $\phi(\rho z)$ function (Pouchou and Pichoir: PAP method)

$\phi(\rho z)$ dependence on Z and E_0



- R_m and R_x
 - decrease with increase in atomic number, Z
 - increase with beam energy, E_0
- $\phi(0)$ increases with beam energy, E_0

X-ray fluorescence

A consequence of X-ray absorption when

$$E_{\text{absorbed X-ray}} > E_{c(\text{absorber shell})}$$

Absorber (Atomic No.)	$E_{K\alpha}$ (keV)	$E_{K\beta}$ (keV)	$E_{c(K)}$ (keV)	$\left(\frac{\mu}{\rho}\right)_{\text{Absorber}}^{NiK\alpha}$ (cm ² /g)
Mn(25)*	5.895	6.492	<u>6.537</u>	<u>344</u>
Fe(26)*	6.4	7.059	<u>7.111</u>	<u>380</u>
Co(27)	6.925	7.649	7.709	53
Ni(28)	<u>7.472</u>	8.265	8.331	59
Cu(29)	8.041	8.907	8.98	65.5

* NiK α fluoresces Mn and Fe

Element	Radiation causing fluorescence
Mn	FeK β , CoK α , CoK β , NiK α , NiK β , CuK α , CuK β
Fe	CoK β , NiK α , NiK β , CuK α , CuK β
Co	NiK β , CuK α , CuK β
Ni	CuK β
Cu	none

Characteristic fluorescence (F) correction

$$\mathbf{F}_i = \frac{\left(1 + \sum_j \left\{ I_{ij}^f / I_i \right\}\right)}{\left(1 + \sum_j \left\{ I_{ij}^f / I_i \right\}\right)^*}$$

* *sample*

I_{ij}^f : intensity of X-ray ν
fluoresced by element j

I_i : intensity of X-ray ν
generated by electron
beam

Fluorescence correction for an element includes the summation of fluoresced intensities by other elements in the compound

F, a function of E_0 and composition

Castaing-Reed method:

$$I_{ij} / I_i = C_j Y_0 Y_1 Y_2 Y_3 P_{ij}$$

$$Y_0 = 0.5[(r_i-1)/r_i][\omega_j A_i/A_j]$$

ω_j : fluorescent yield

$$Y_1 = [(U_j-1)/(U_i-1)]^{1.67}$$

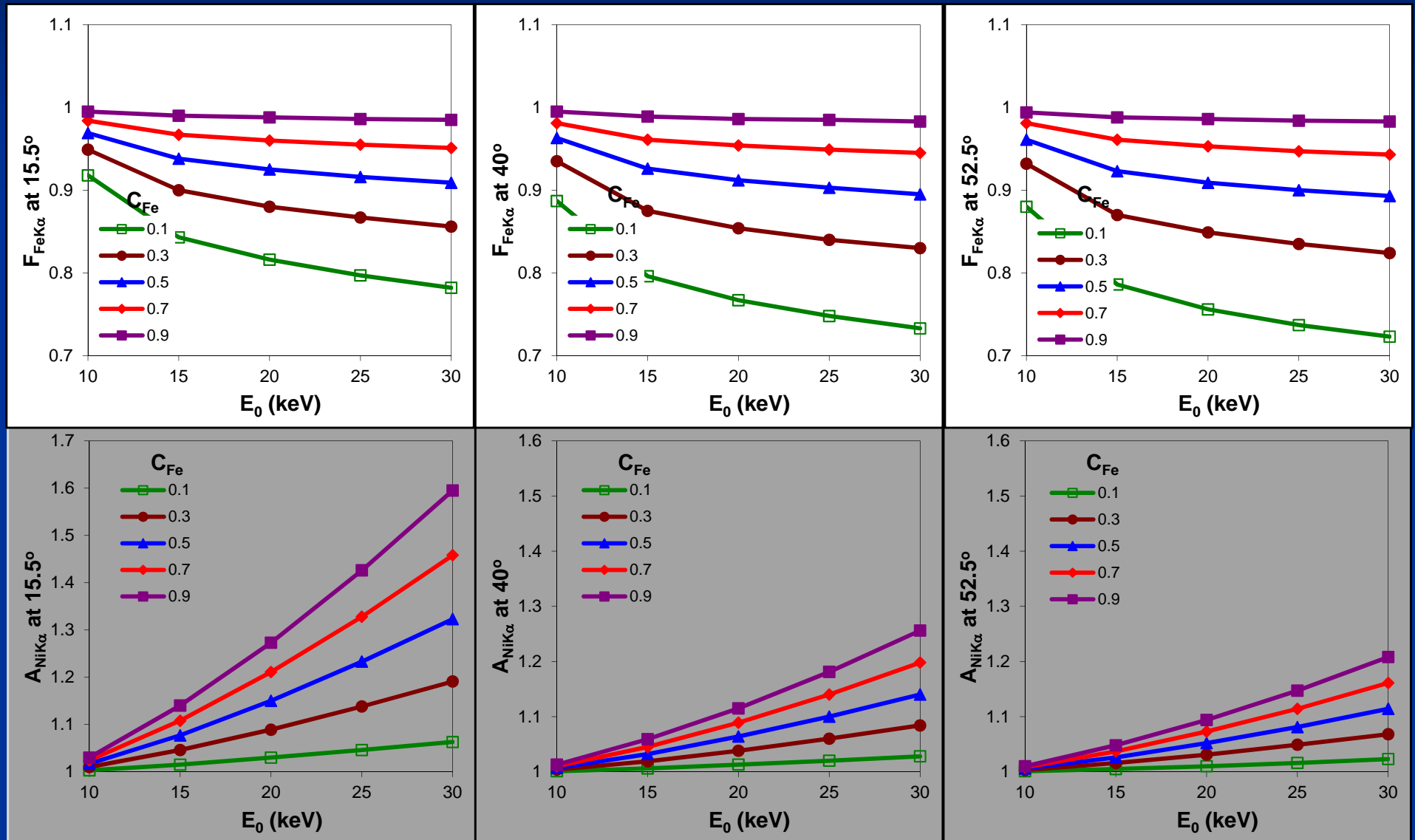
$$Y_2 = (\mu/\rho)_i^j / (\mu/\rho)_{\text{spec}}^j$$

$$Y_3 = [\ln(1+u)]/u + [\ln(1+v)]/v$$
$$u = [(\mu/\rho)_{\text{spec}}^j / (\mu/\rho)_{\text{spec}}^j] \operatorname{cosec} \psi$$
$$v = 3.3 \times 10^5 / [(E_0^{1.65} - E_c^{1.65}) (\mu/\rho)_{\text{spec}}^j]$$

$P_{ij}=1$ for K fluorescing K;
4.76 for K fluorescing L;
0.24 for L fluorescing K

F, a function of E_0 and composition

$F_{\text{FeK}\alpha}$ in Fe-Ni alloy



$A_{\text{NiK}\alpha}$ in Fe-Ni alloy

Matrix correction flowchart

Concentrations are calculated through an iterative procedure:

$$k \text{ -----} \rightarrow ZAF_1 \text{ -----} \rightarrow C_1 (= k * ZAF_1)$$

$$C_1 \text{ -----} \rightarrow ZAF_2 \text{ -----} \rightarrow C_2 (= k * ZAF_2) \quad (\text{if } C_2 = C_1, \text{ stop here})$$

$$C_2 \text{ -----} \rightarrow ZAF_3 \text{ -----} \rightarrow C_3 (= k * ZAF_3) \quad (\text{if } C_3 = C_2, \text{ stop here})$$

and so on....

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