

Using

$$\frac{\partial T}{\partial s^*} = \frac{\partial T}{\partial M} \frac{dM}{ds^*},$$

We can re-write (18) as

$$\frac{\partial T_o}{\partial M} \cong -\frac{Ri_c}{r_t^2} \left(\frac{dM}{ds^*} \right). \quad (19)$$

We can also re-write (6) as

$$M_b = r_b^2 \left(\frac{1}{2} f - (T_b - T_o) \frac{ds^*}{dM} \right) \quad (20)$$

Boundary layer
entropy

$$h \frac{ds_b}{dt} = C_k |\mathbf{V}| (s_0^* - s_b) + C_d \frac{|\mathbf{V}|^3}{T_b} \quad (21)$$

Boundary layer
angular momentum

$$h \frac{dM}{dt} = -r |\mathbf{V}| V \quad (22)$$

Combine (21) and (22):

$$\frac{ds_b}{dM} = -\frac{C_k}{C_D} \frac{(s_0^* - s_b)}{rV} - \frac{|\mathbf{V}|^2}{T_b rV}$$

Let $s_b \simeq s^*$, $|\mathbf{V}| \simeq V \simeq V_b$, $r \simeq r_b$

$$\rightarrow \frac{ds^*}{dM} = -\frac{C_k}{C_D} \frac{(s_0^* - s^*)}{r_b V_b} - \frac{V_b}{T_b r_b} \quad (23)$$

Balance condition (8):

$$\frac{V_b}{r_b} = -(T_b - T_o) \frac{ds^*}{dM} \quad (24)$$

Eliminate V_b between (23) and (24):

$$\left(\frac{ds^*}{dM}\right)^2 = \frac{T_b C_k}{T_o C_D} \frac{(s_0^* - s^*)}{r_b^2 (T_b - T_o)} \quad (25)$$

Eliminate r_b^2 between (20) and (25):

$$\left(\frac{ds^*}{dM}\right)^2 + 2\chi \frac{ds^*}{dM} - \frac{\chi f}{T_b - T_o} = 0, \quad (26)$$

where

$$\chi \equiv \frac{T_b C_k}{T_o C_D} \frac{s_0^* - s^*}{2M}$$

Remember that

$$\frac{\partial T_o}{\partial M} \cong -\frac{Ri_c}{r_t^2} \left(\frac{dM}{ds^*}\right) \quad (19)$$

Integrate (26) and (19) inward from some outer radius r_o , defined such that

$$V = 0 \quad \text{at} \quad r = r_o$$

In general, integrating this system will not yield $T_o = T_t$ at $r = r_{max}$. Iterate value of r_t until this condition is met.

If $V \gg fr$, we ignore dissipative heating, and we neglect pressure dependence of s_o^* , then we can derive an approximate closed-form solution.

Assuming that Ri is critical in the outflow leads to an equation for T_0 that, coupled to the interior balance equation and the slab boundary layer lead (surprisingly!) to a closed form analytic solution for the gradient wind (as represented by angular momentum, M , at the top of the boundary layer:

$$\left(\frac{M}{M_m}\right)^{2-\frac{C_k}{C_D}} = \frac{2\left(\frac{r}{r_m}\right)^2}{2-\frac{C_k}{C_D} + \frac{C_k}{C_D}\left(\frac{r}{r_m}\right)^2}, \quad (27)$$

$$\left(\frac{fr_o^2}{2V_m r_m} \right)^{2-\frac{C_k}{C_D}} = \frac{2 \left(\frac{r_o}{r_m} \right)^2}{2 - \frac{C_k}{C_D} + \frac{C_k}{C_D} \left(\frac{r_o}{r_m} \right)^2}. \quad (28)$$

$$r_m \cong \frac{1}{2} fr_o^2 V_m^{-1} \left(\frac{1}{2} \frac{C_k}{C_D} \right)^{\frac{1}{2-\frac{C_k}{C_D}}} \quad (29)$$

The maximum wind speed, V_m , found from maximizing the radial dependence of wind speed in the solution (27) is given by

$$V_m^{2-\frac{C_k}{C_D}} = V_p^2 \left(\frac{2r_m}{fr_o^2} \right)^{\frac{C_k}{C_D}} \quad (30)$$

$$V_p^2 \equiv \frac{C_k}{C_D} (T_b - T_t) (s_0^* - s_e^*)$$

Substituting (29) into (30) gives

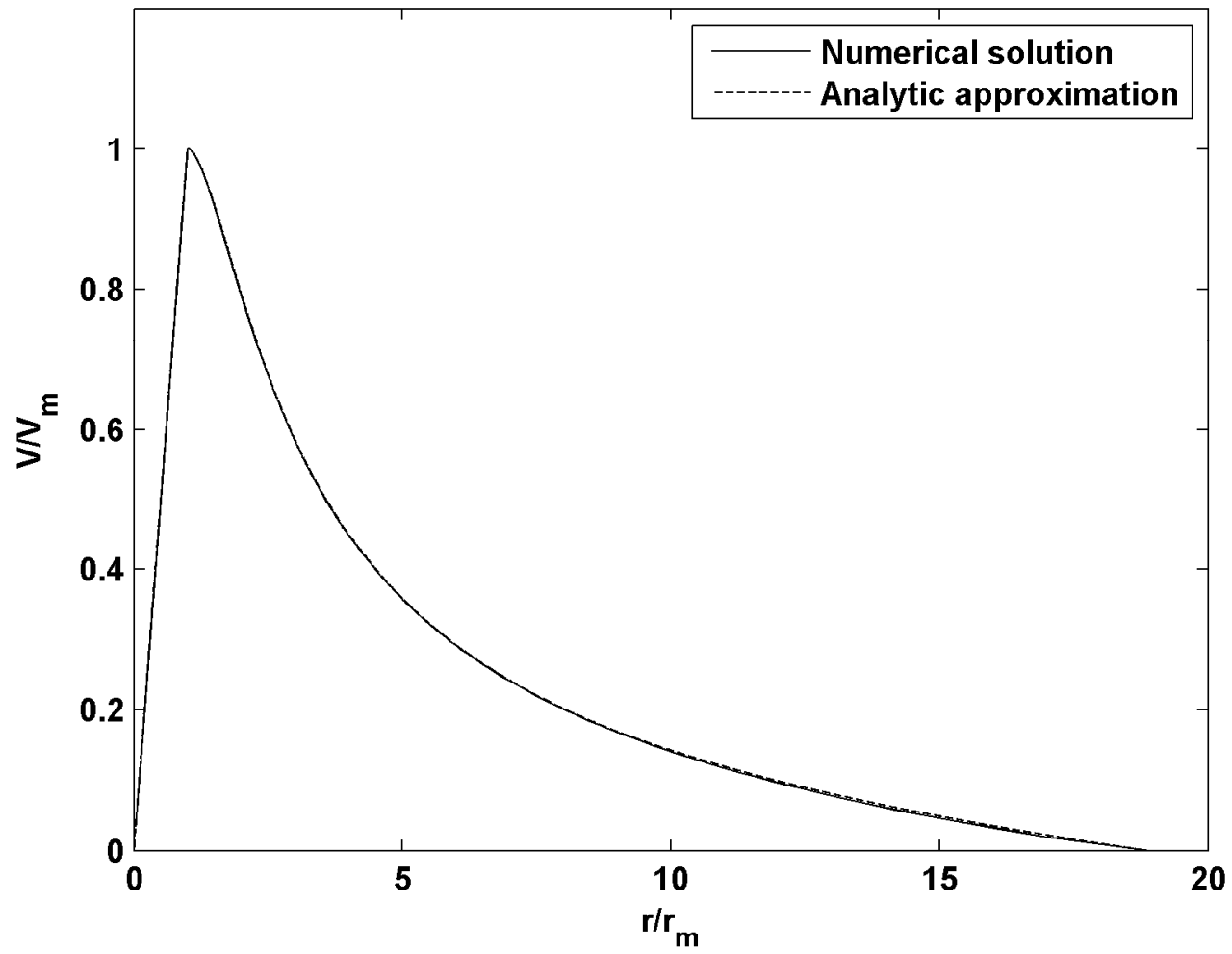
$$V_m^2 \cong V_p^2 \left(\frac{1}{2} \frac{C_k}{C_D} \right)^{\frac{\frac{C_k}{C_D}}{2 - \frac{C_k}{C_D}}} \quad (31)$$

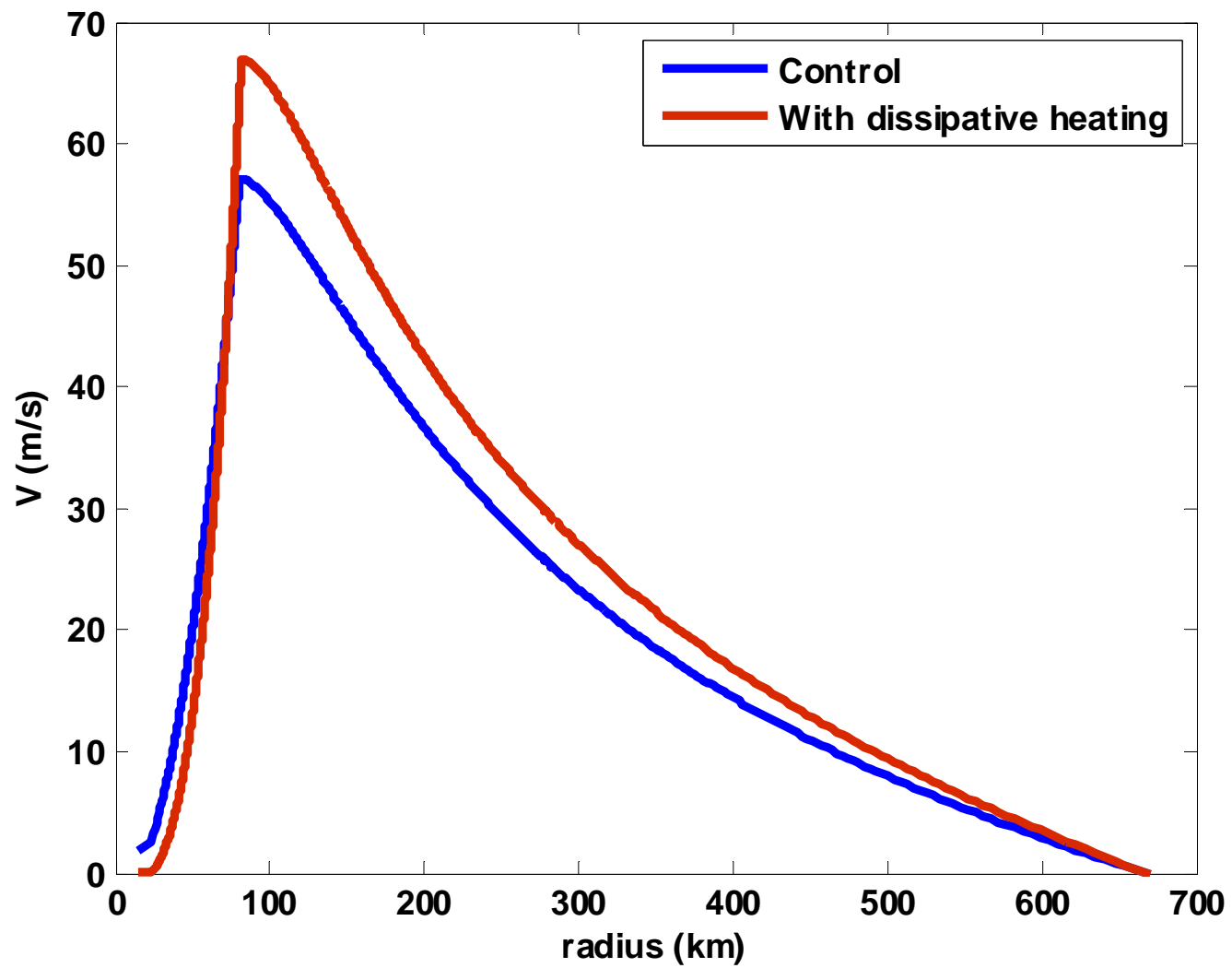
Substituting (31) into (29) gives

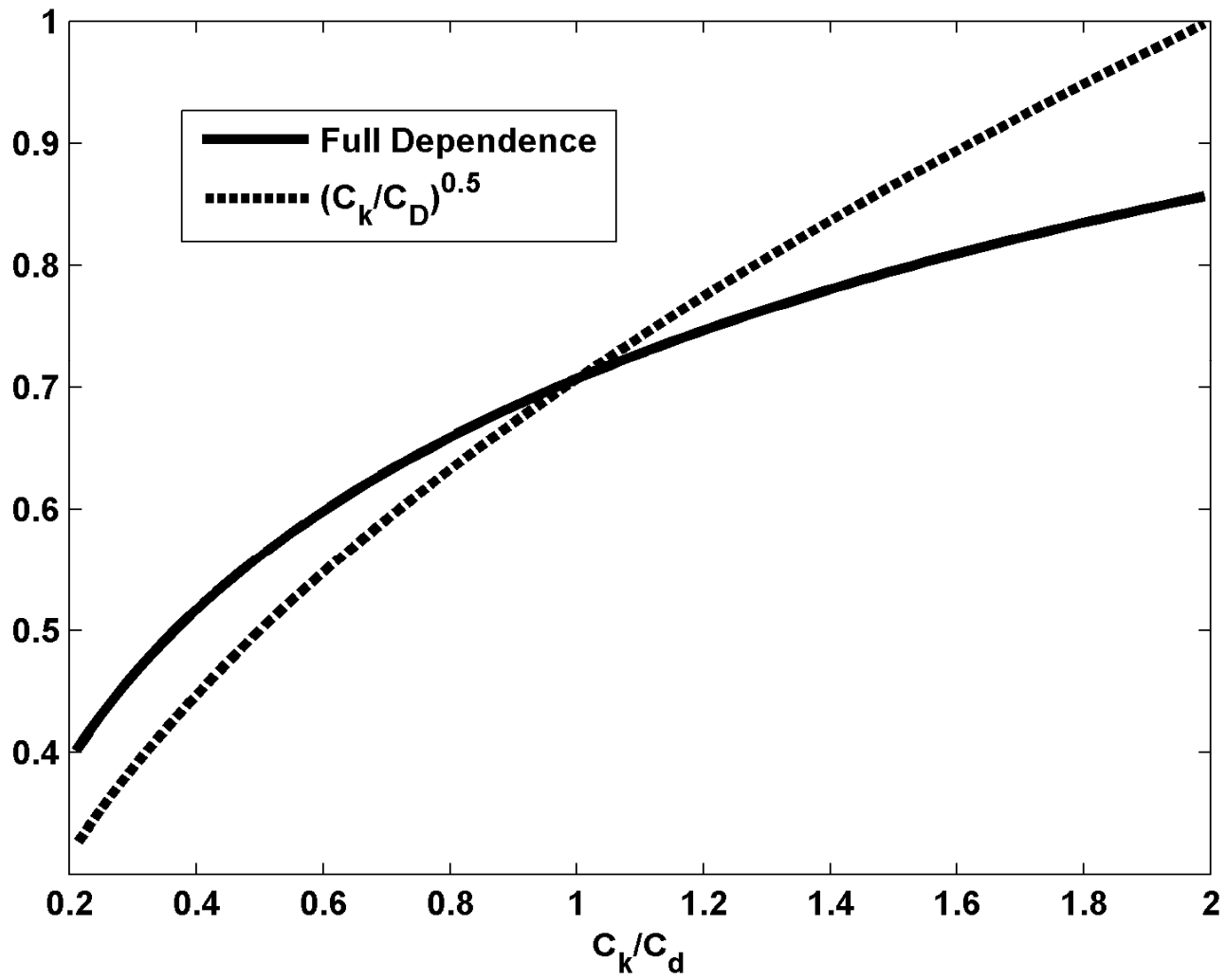
$$r_m \cong \left(\frac{1}{2} \right)^{\frac{3}{2}} \frac{f r_o^2}{\sqrt{(T_b - T_t)(s_o^* - s_e^*)}}$$

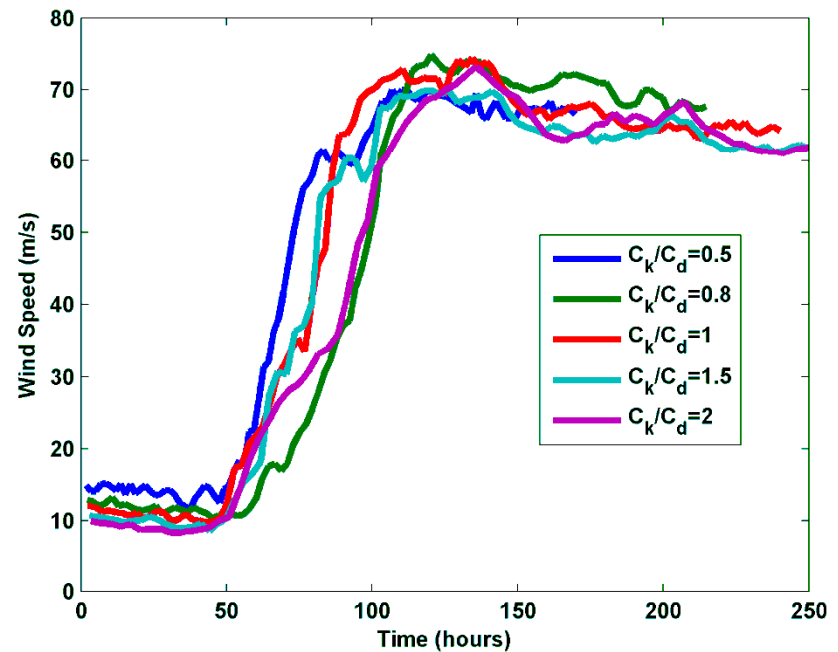
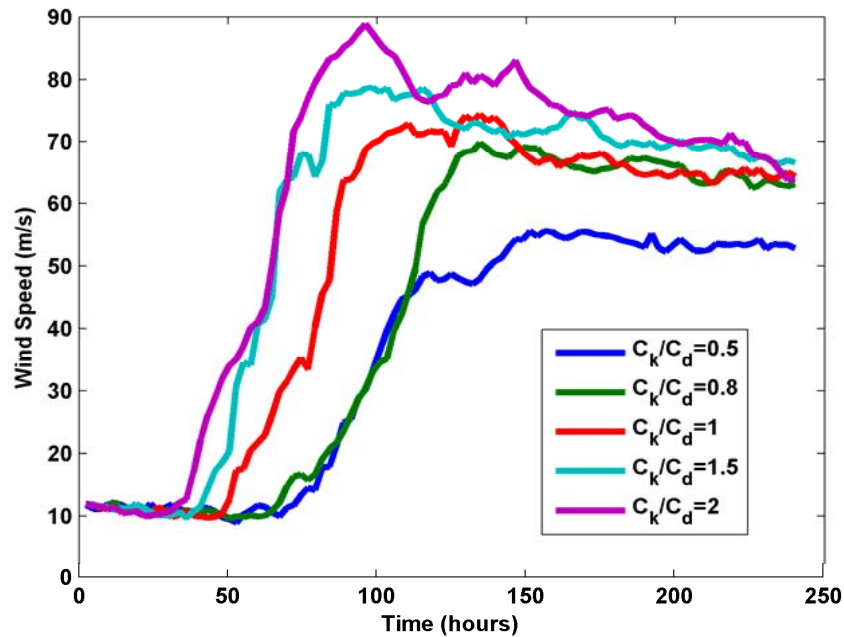
Also,

$$r_t^2 = r_m^2 \frac{C_D}{C_k} Ri_c$$





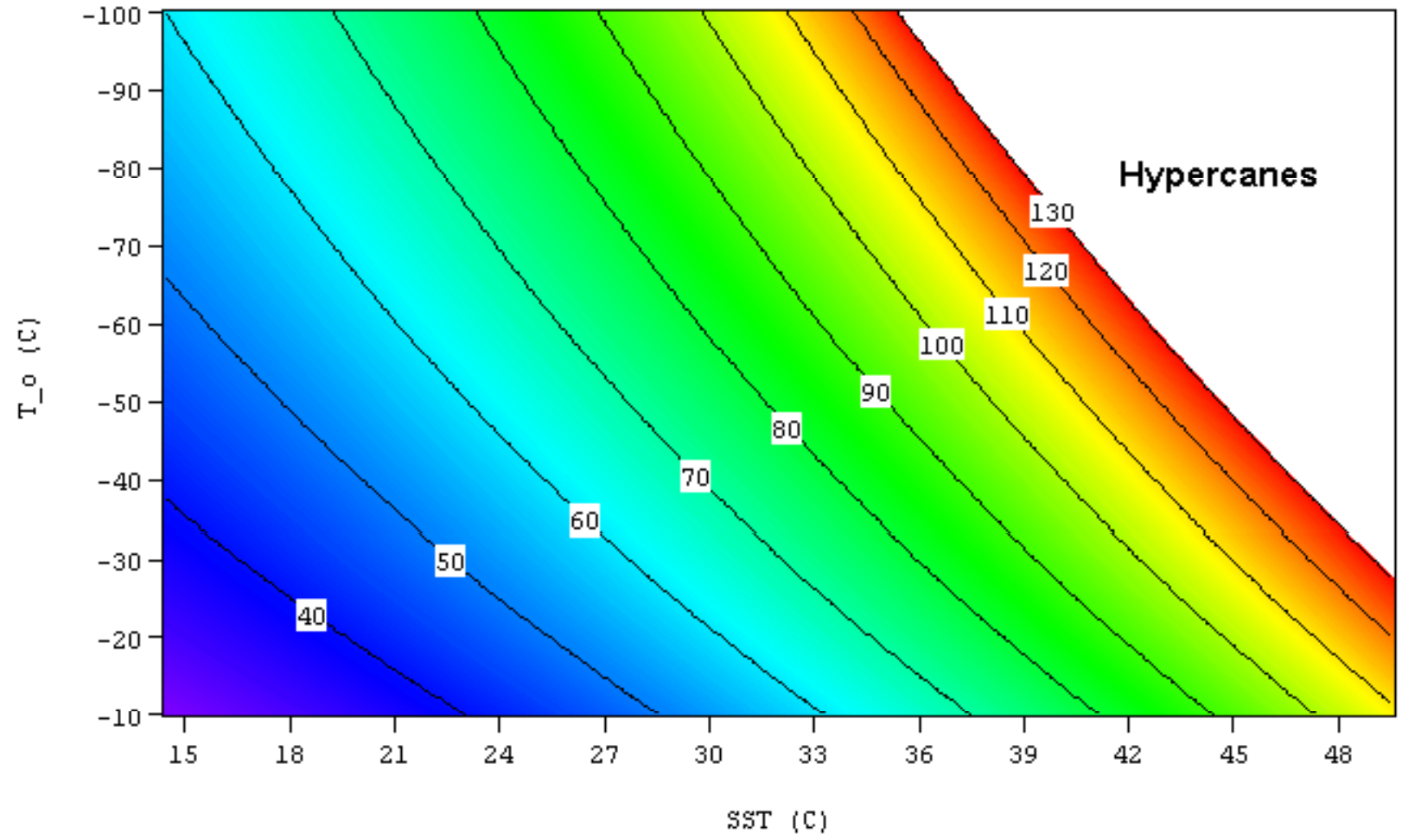




Numerical integrations with RE87 model (no dissipative heating, no pressure dependence of k_0^*) : Left, regular variables; Right: Velocity scaled by (31) and time scaled by the inverse square-root of the enthalpy exchange coefficient.

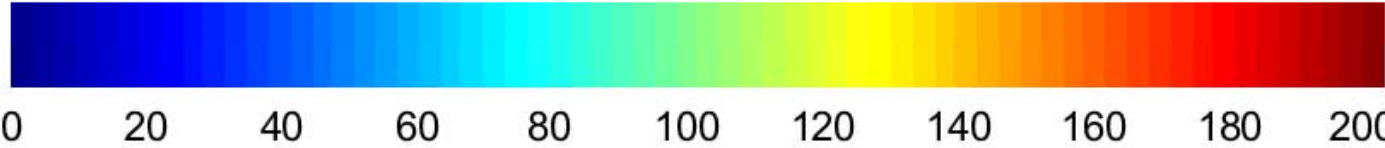
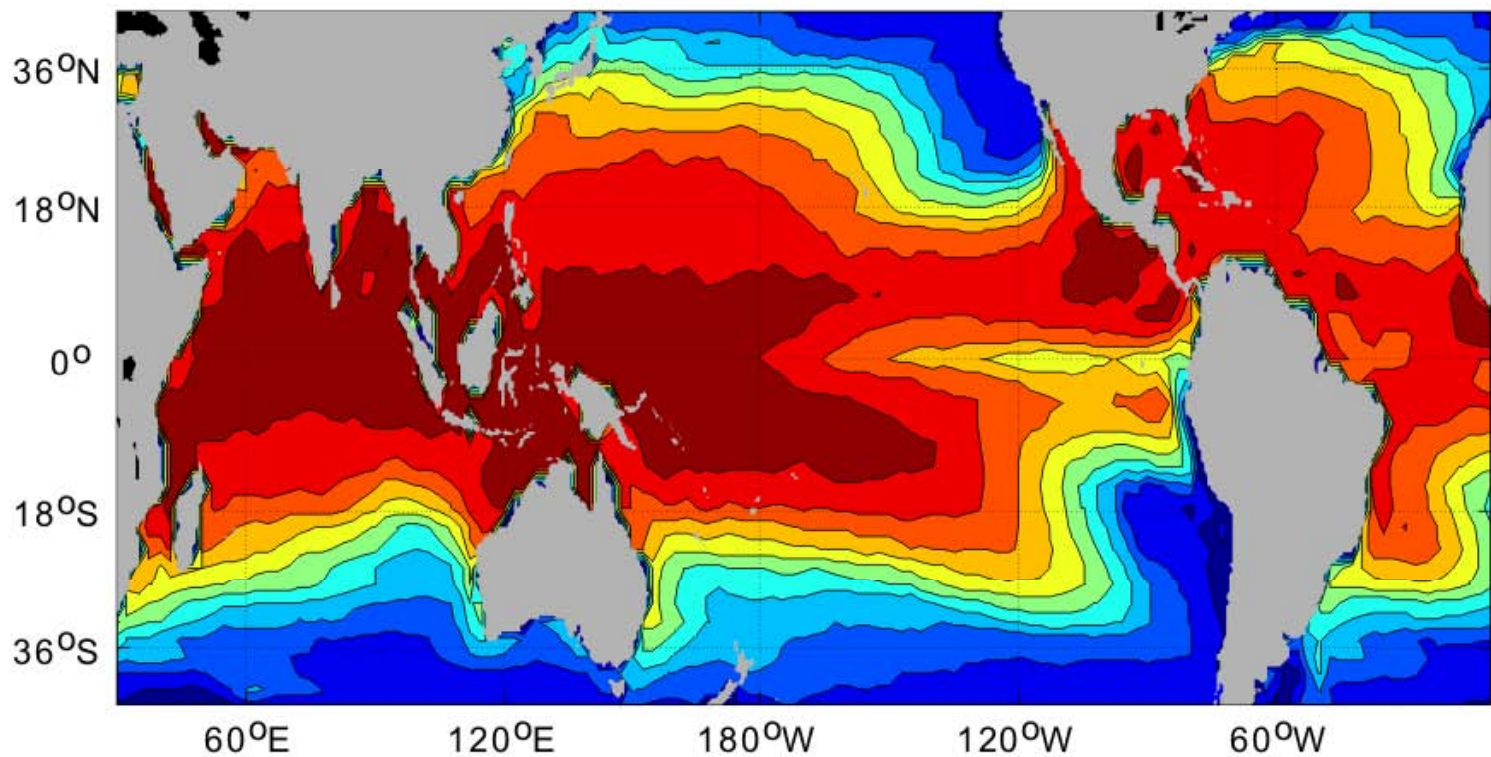
Effects of Pressure-Dependence of Surface Saturation Enthalpy

Maximum Wind Speed (m/s)

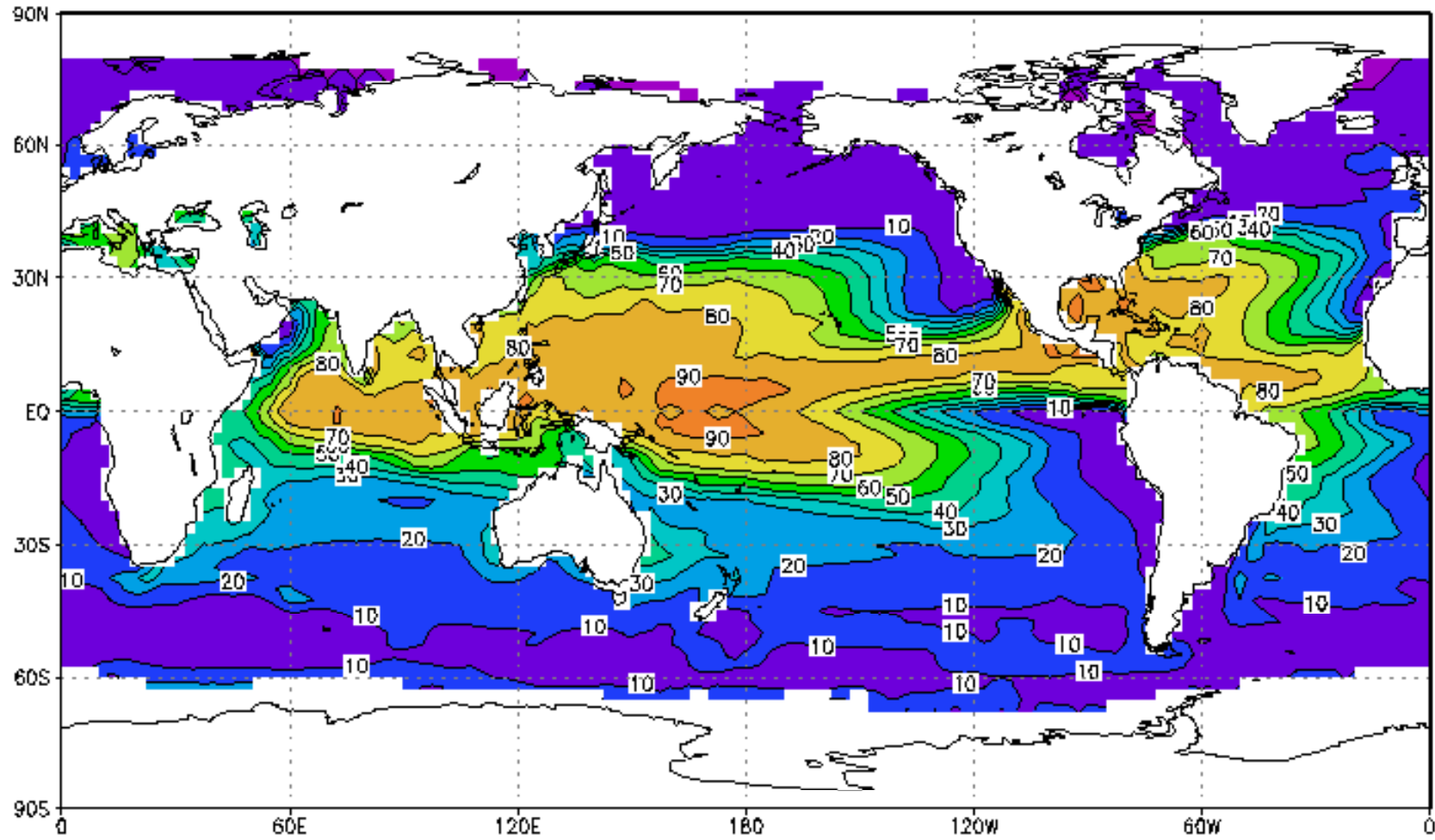


$$\mathcal{R} = 0.75 \quad C_k/C_D = 1.2$$

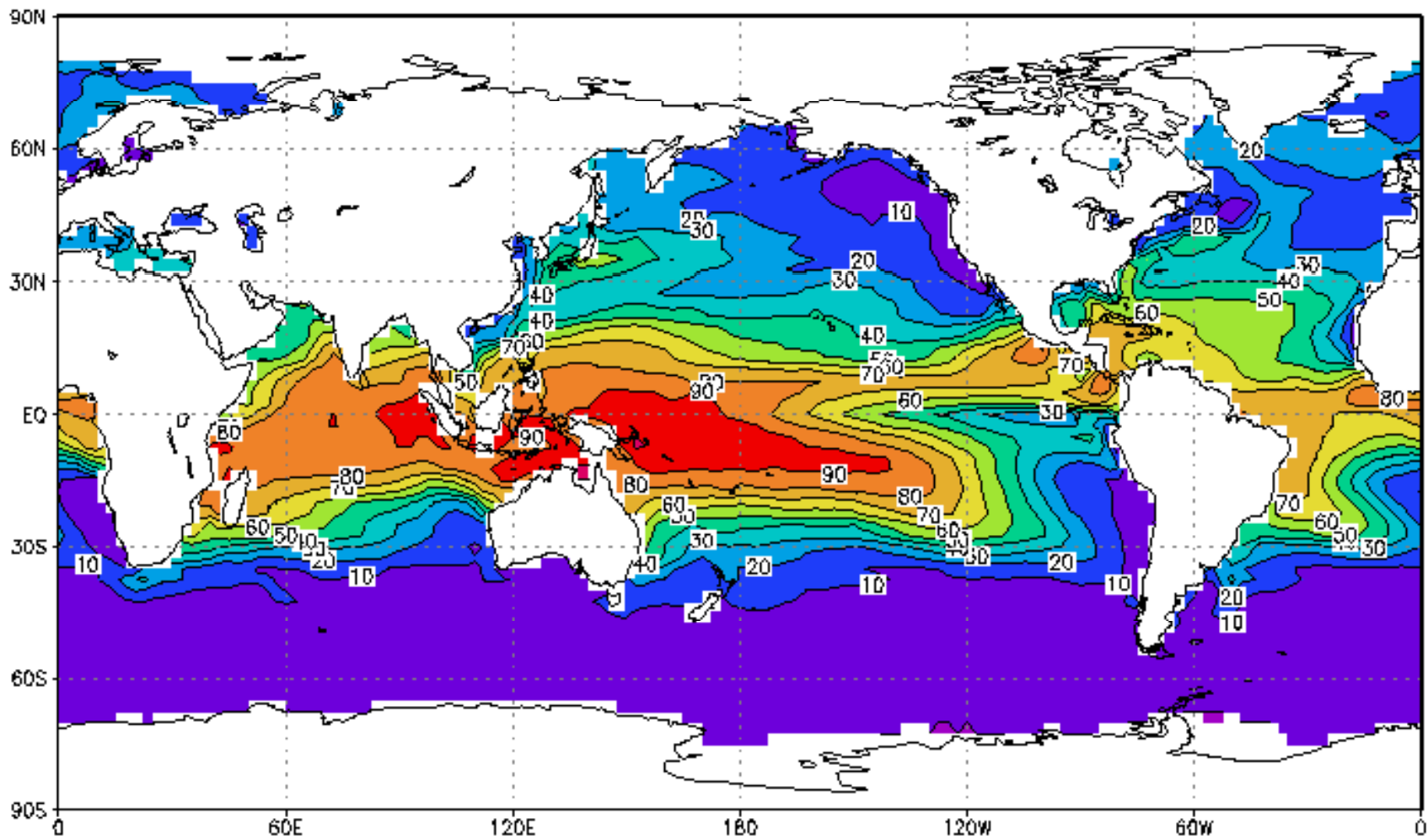
Maximum Annual Potential Intensity (MPH)



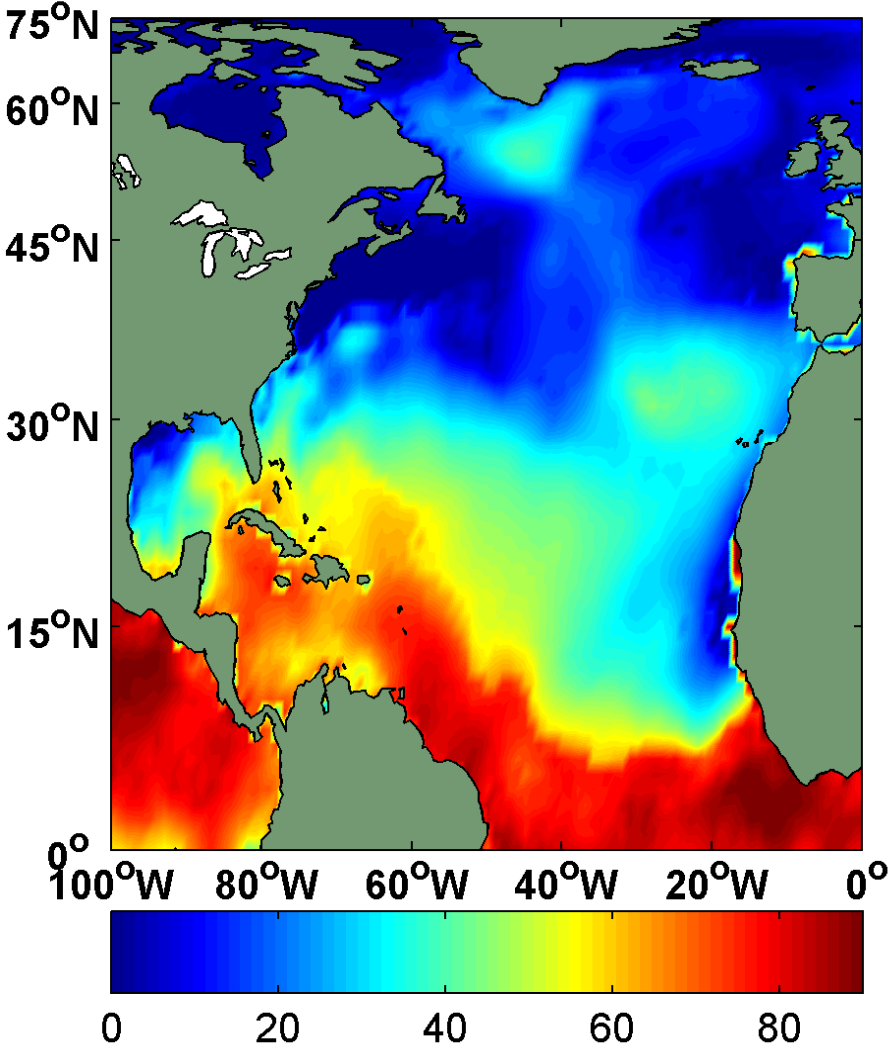
AUGUST MEAN



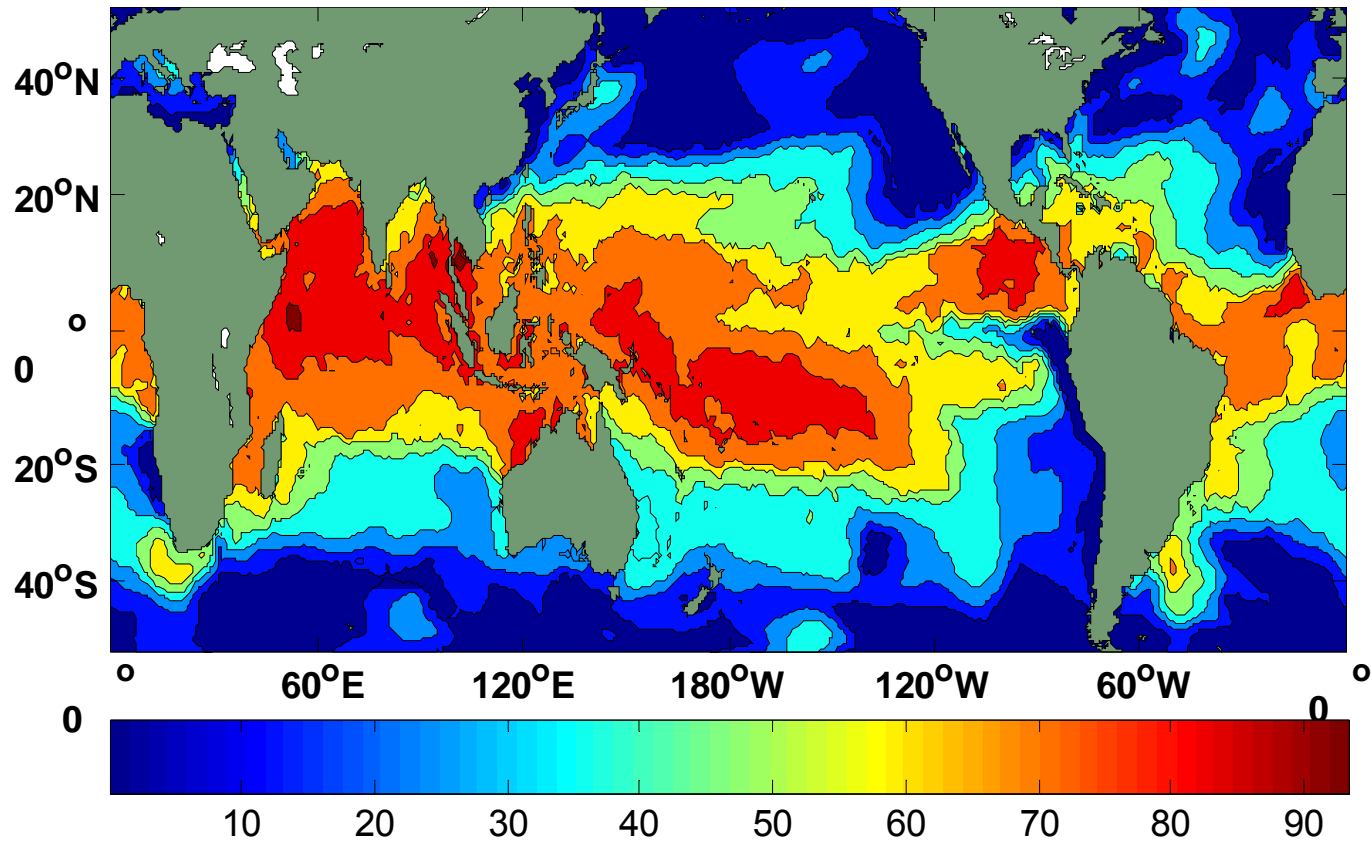
JANUARY MEAN



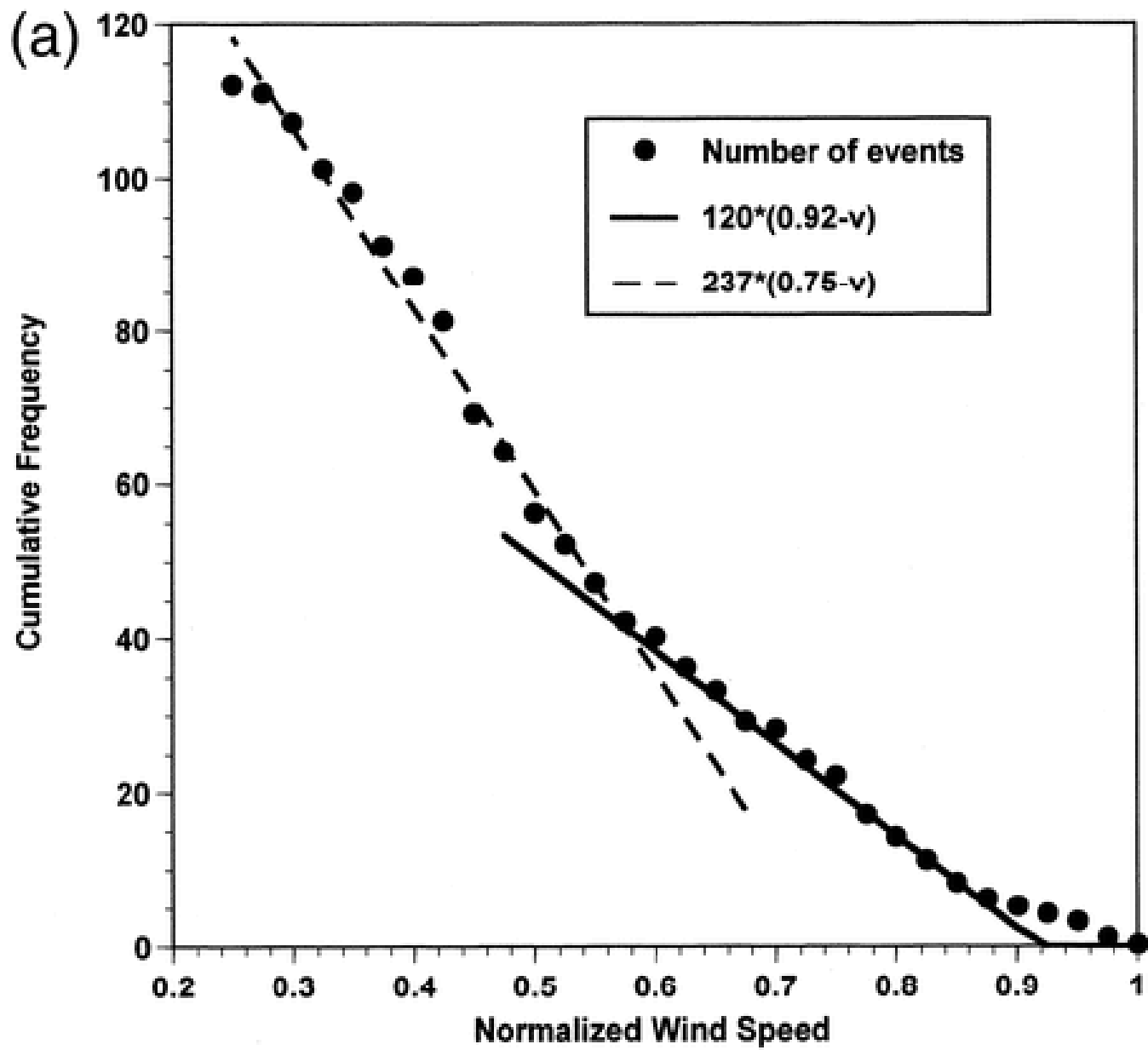
27 April 2011 12 GMT

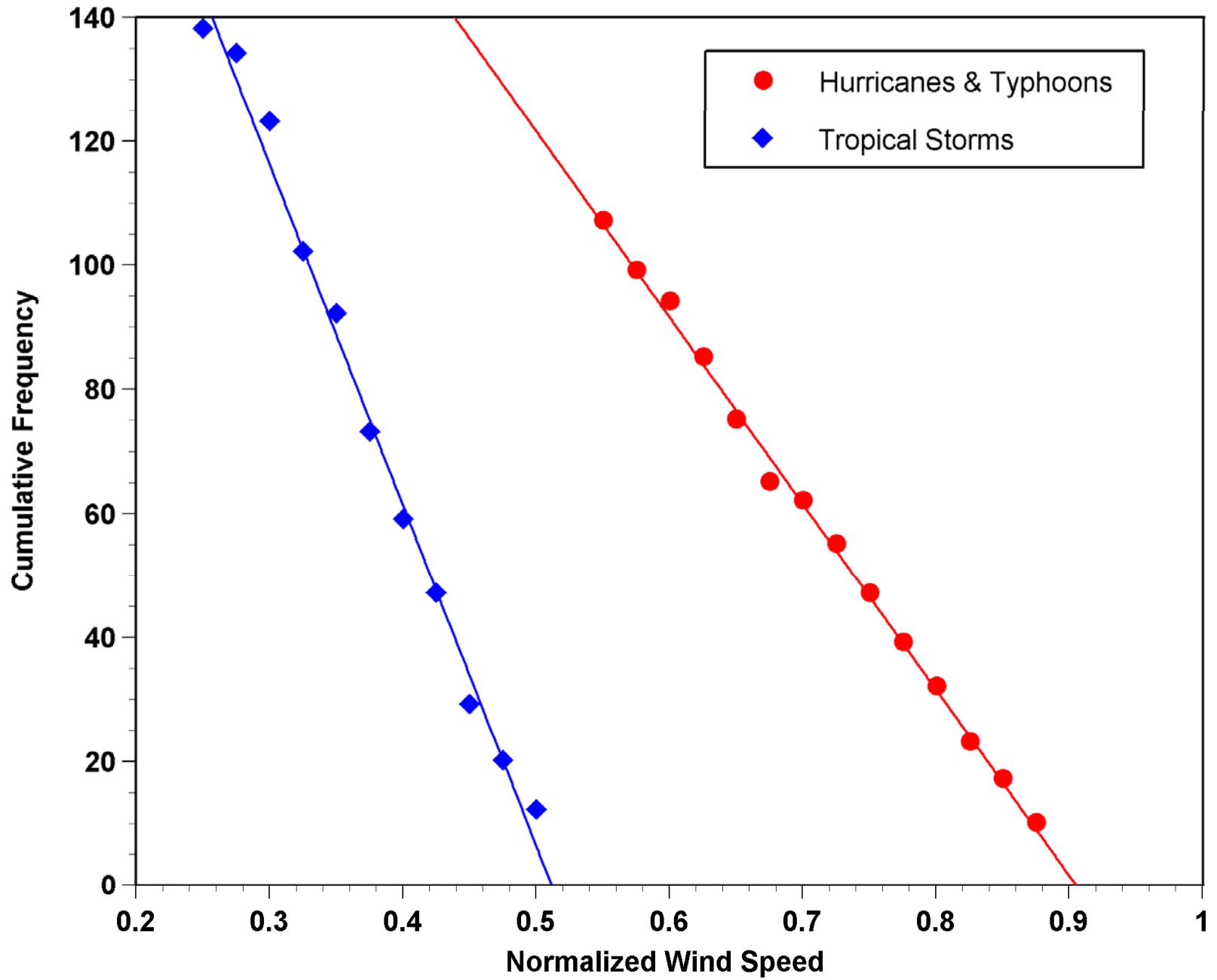


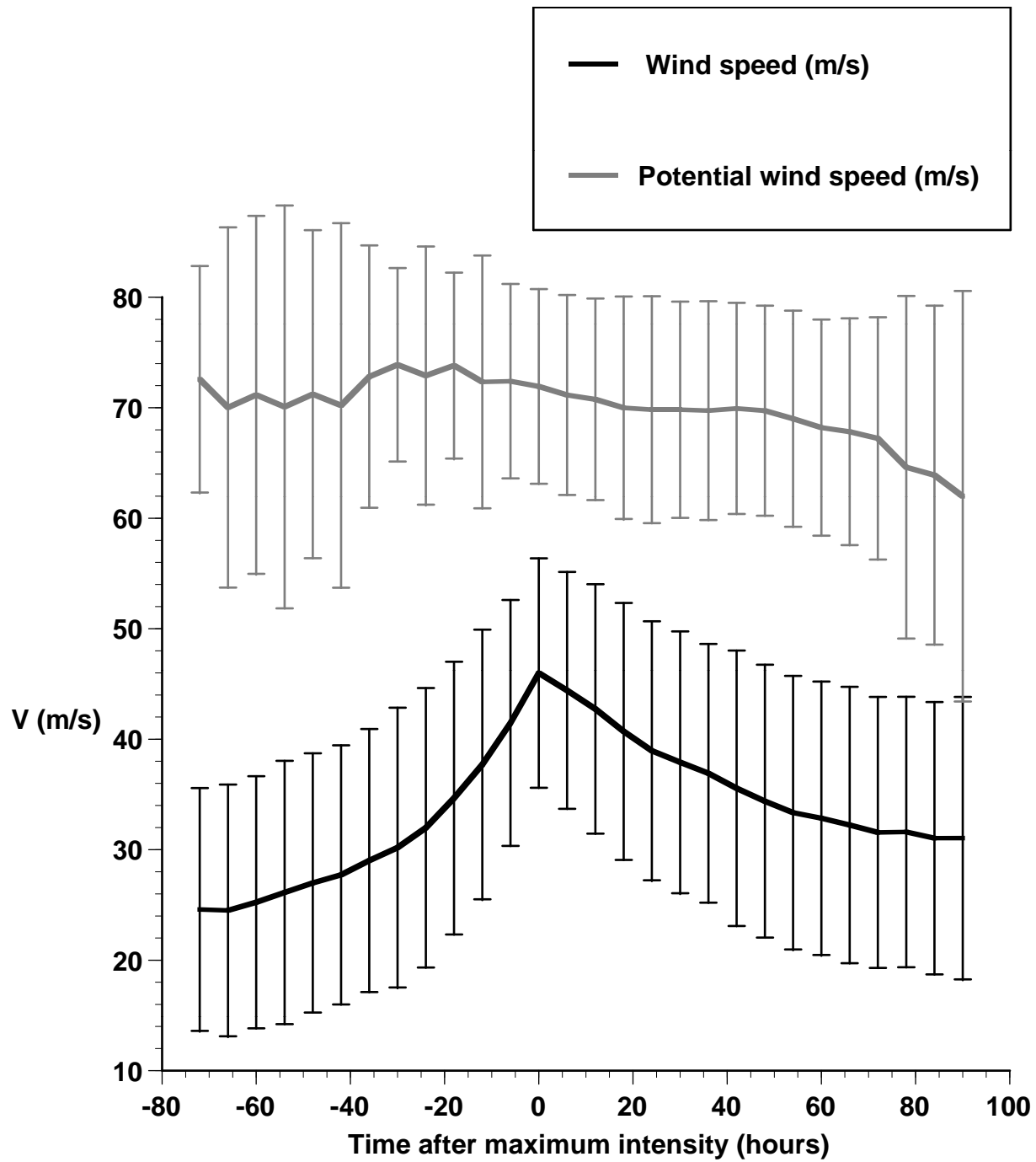
00 GMT 27 April 2007



Relationship between potential intensity (PI) and intensity of real tropical cyclones

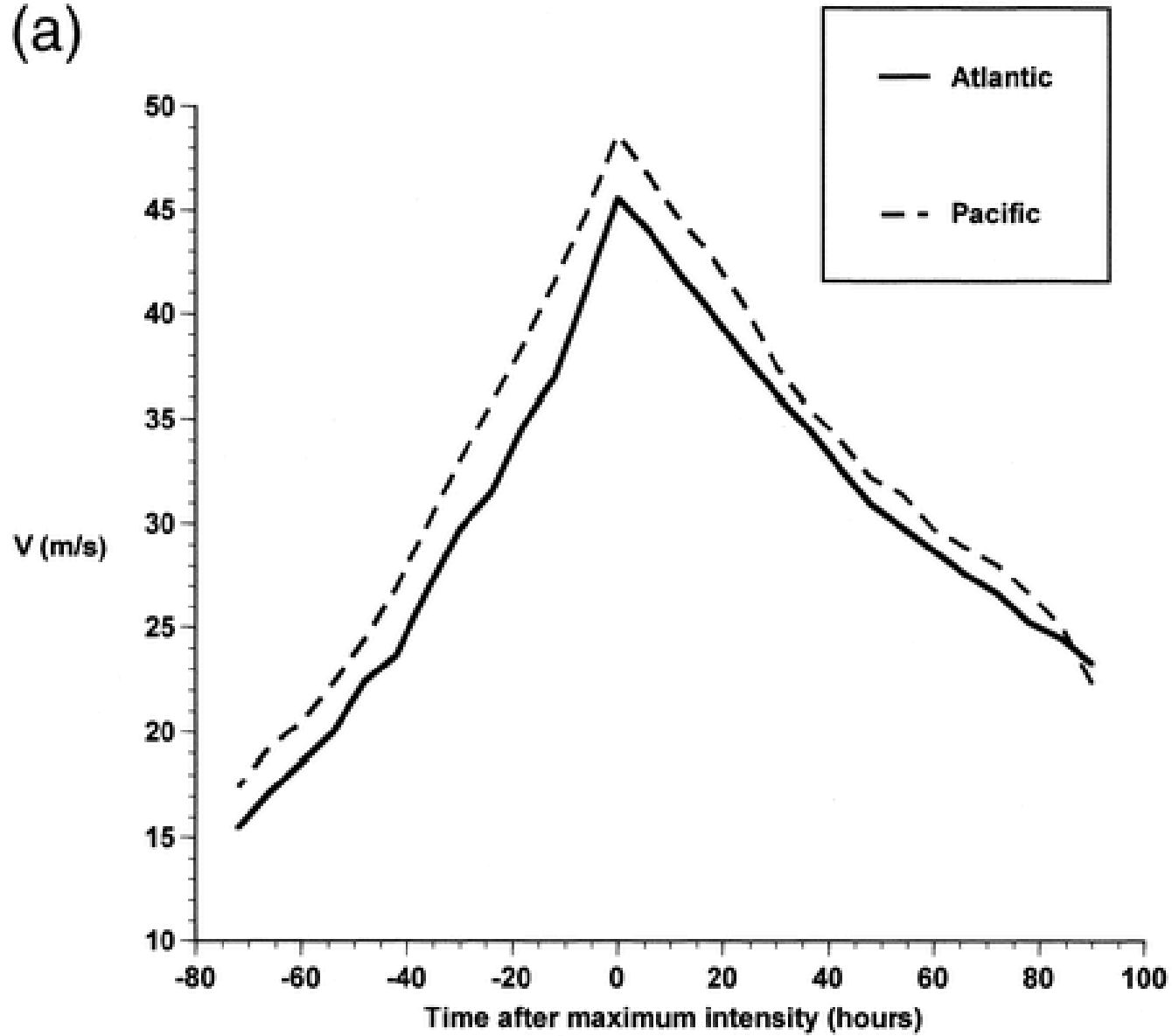




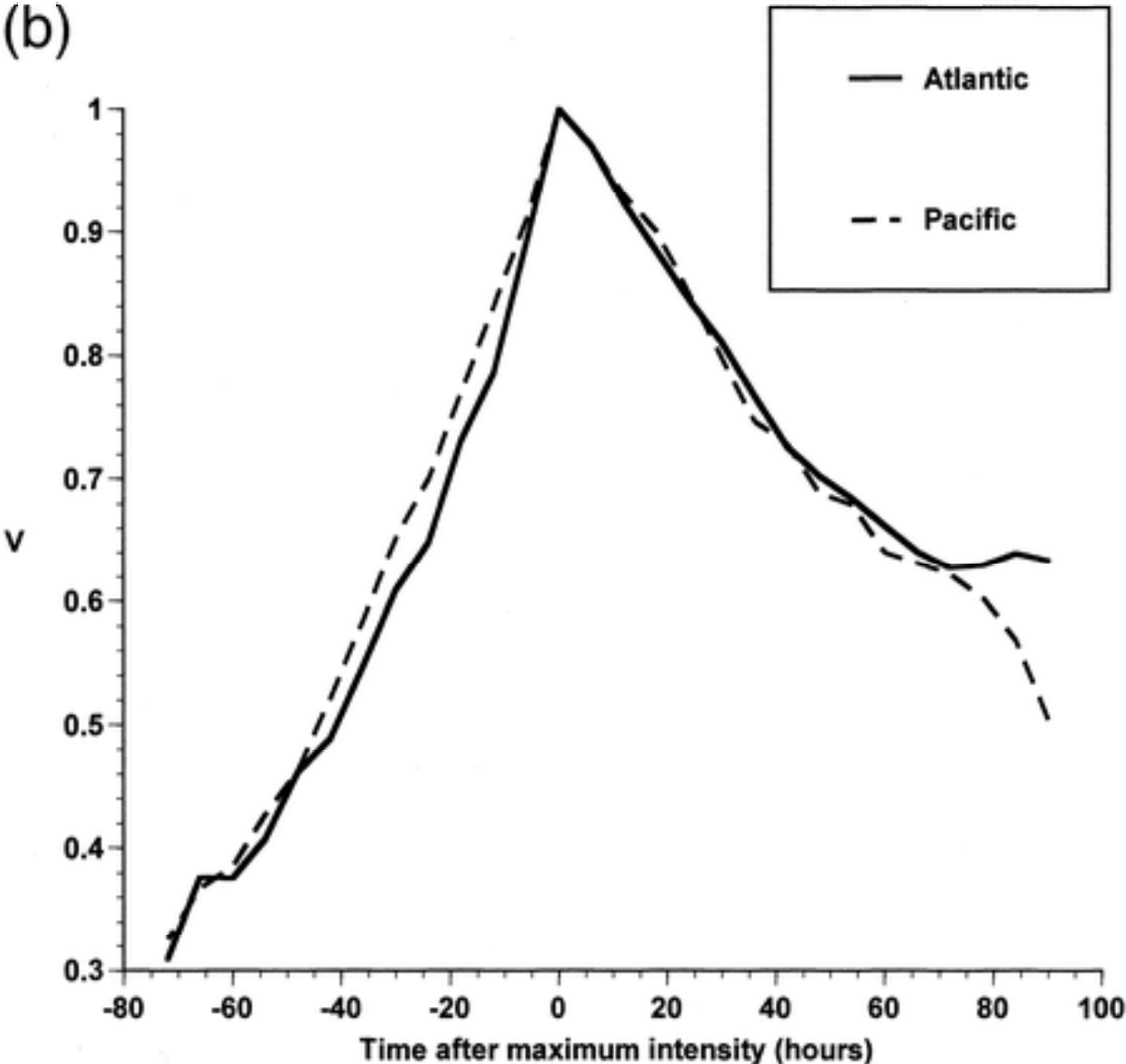


Evolution with respect to time of maximum intensity

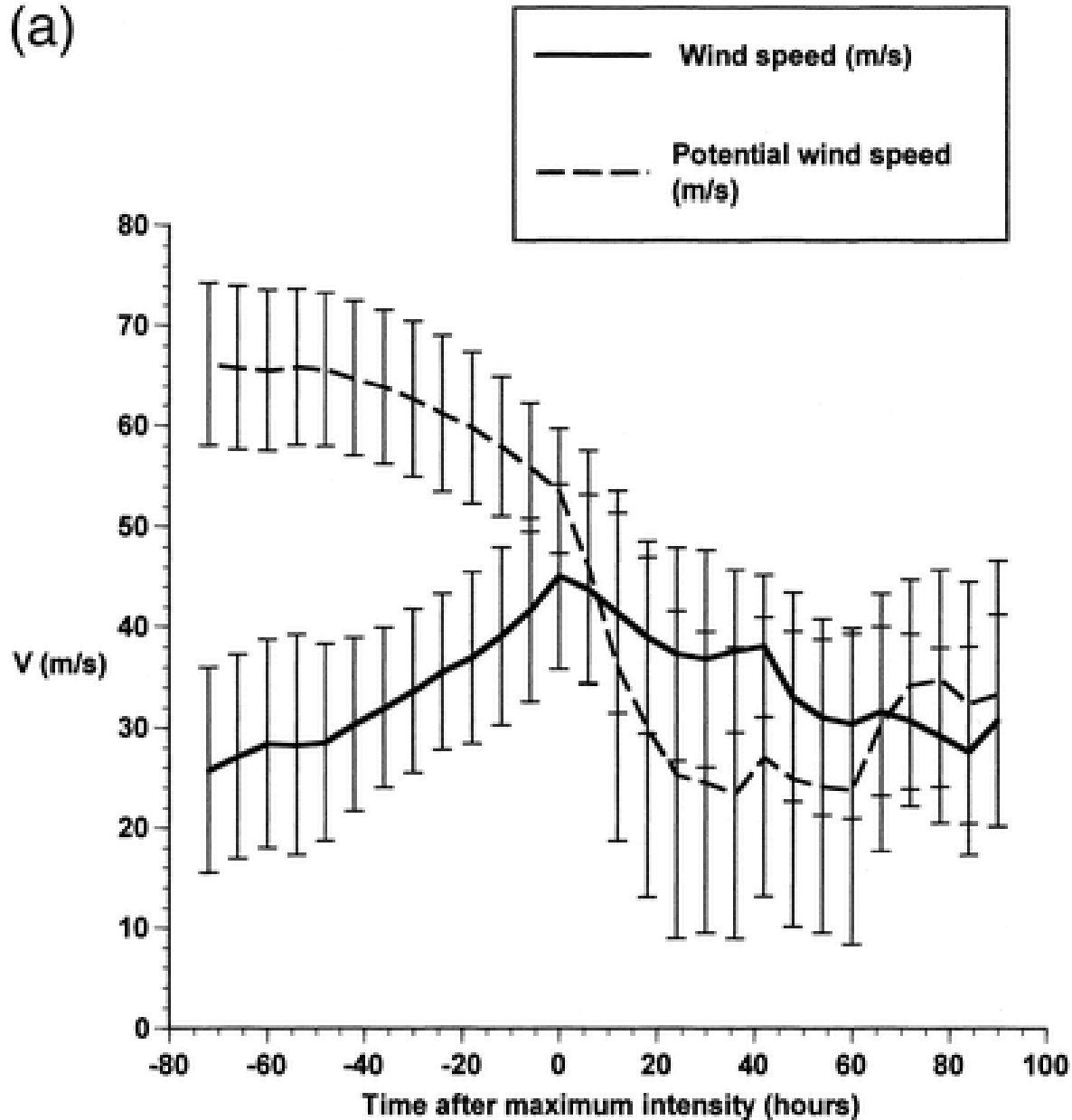
(a)



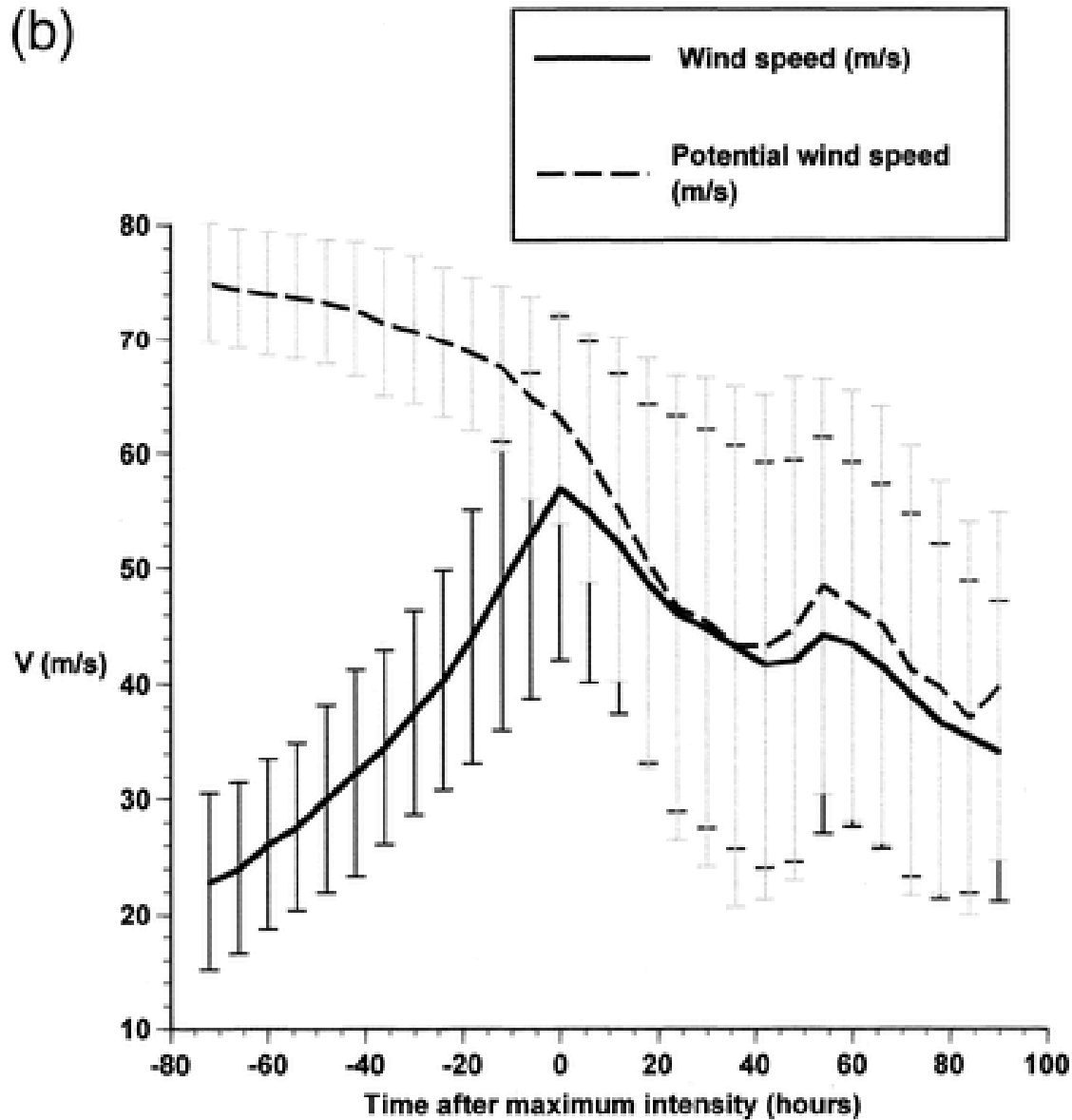
Evolution with respect to time of maximum intensity, normalized by peak wind



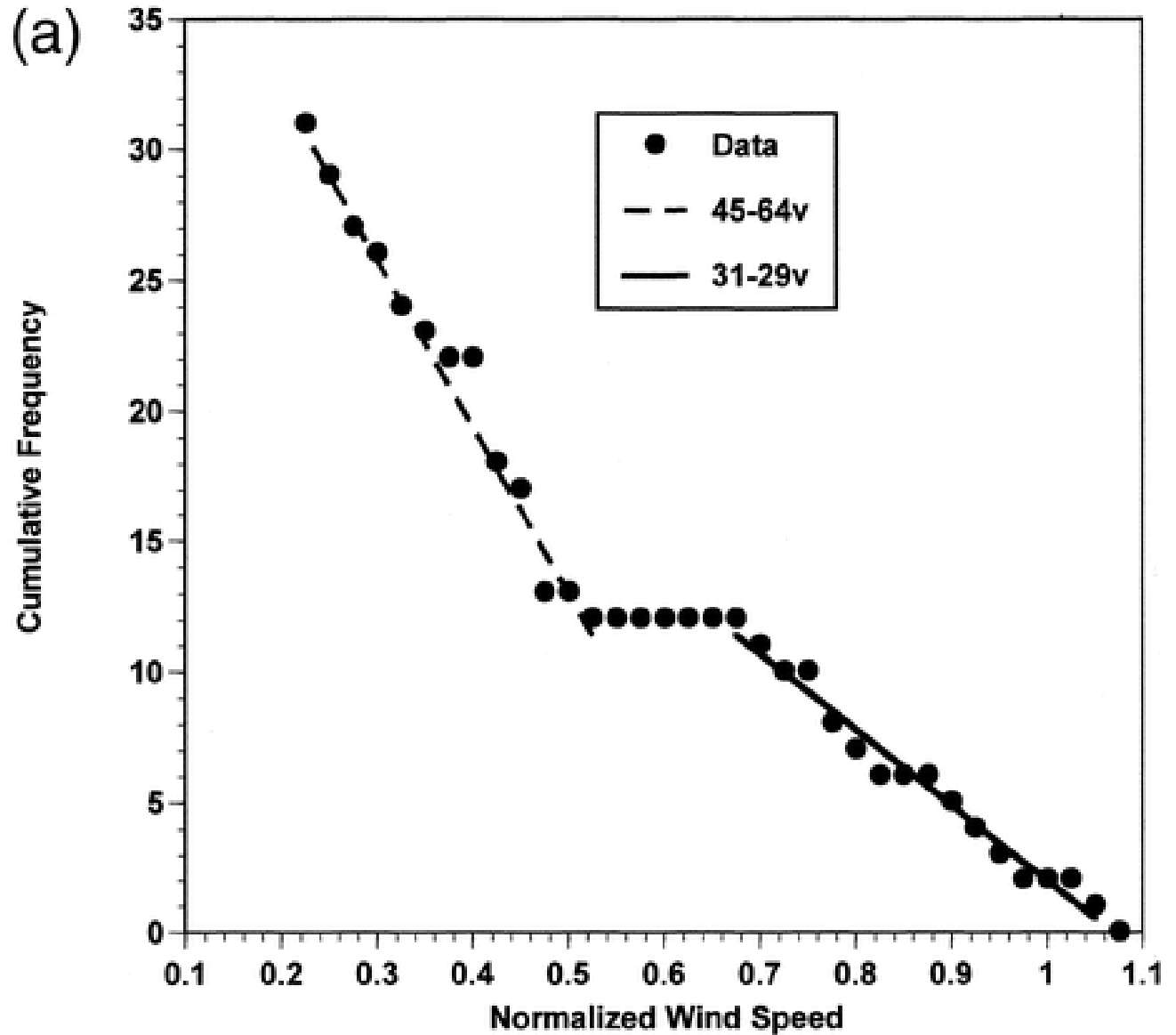
Evolution curve of Atlantic storms whose lifetime maximum intensity is limited by declining potential intensity, but not by landfall (a)



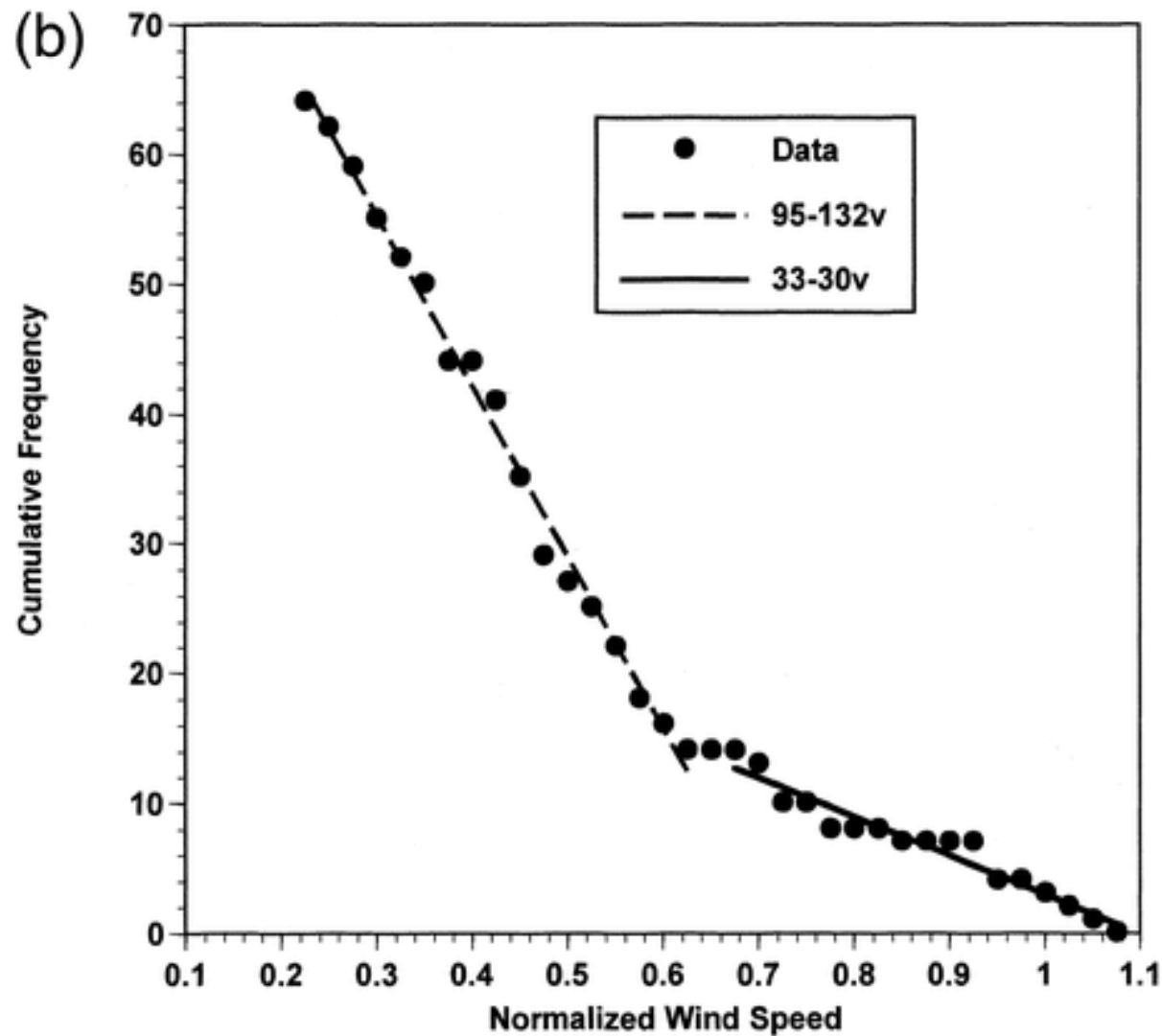
Evolution curve of WPAC storms whose lifetime maximum intensity is limited by declining potential intensity, but not by landfall



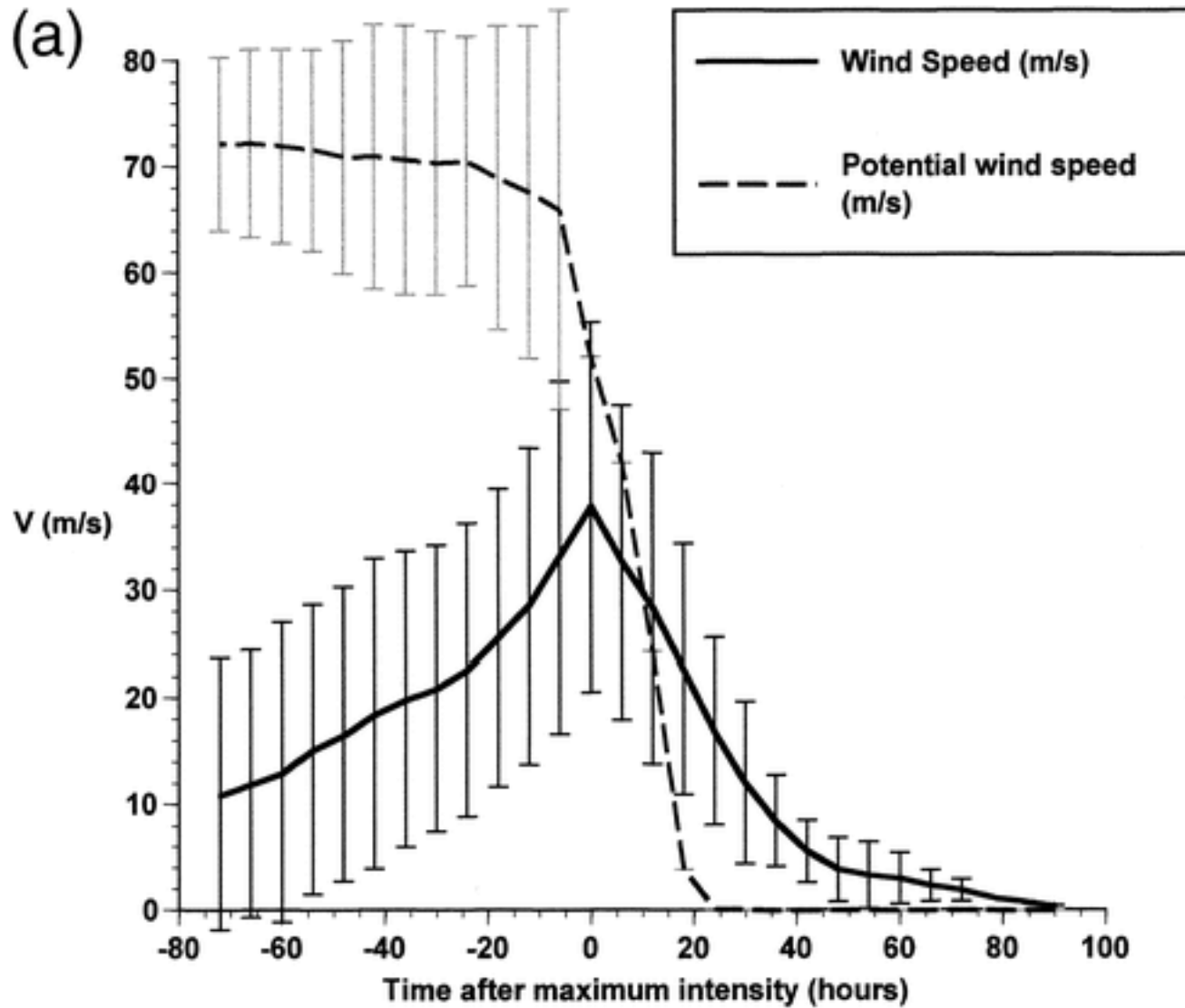
CDF of normalized lifetime maximum wind speeds of North Atlantic tropical cyclones of tropical storm strength (18 m s^{-1}) or greater, for those storms whose lifetime maximum intensity was limited by landfall. (a)



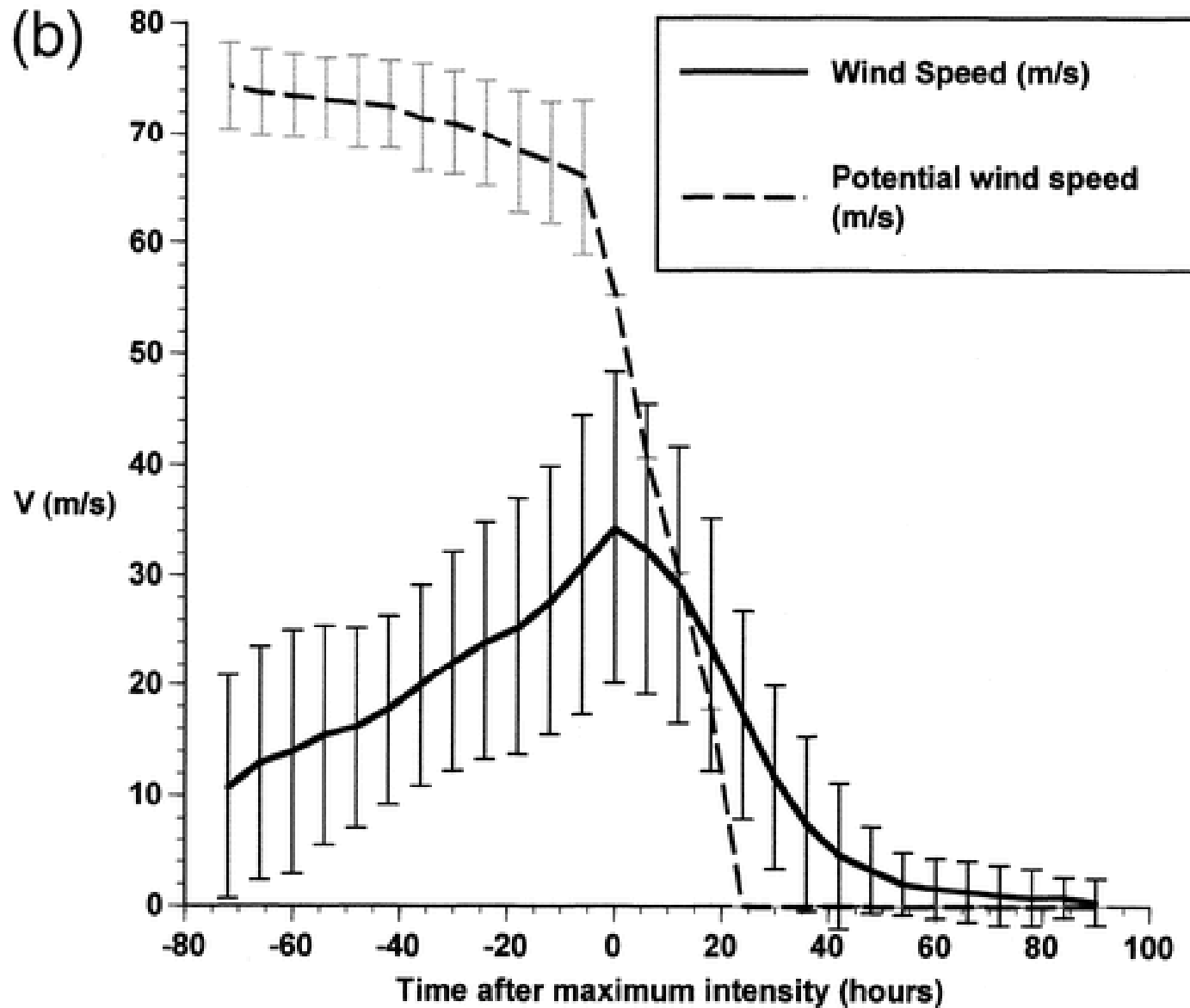
CDF of normalized lifetime maximum wind speeds of Northwest Pacific tropical cyclones of tropical storm strength (18 m s^{-1}) or greater, for those storms whose lifetime maximum intensity was limited by landfall.



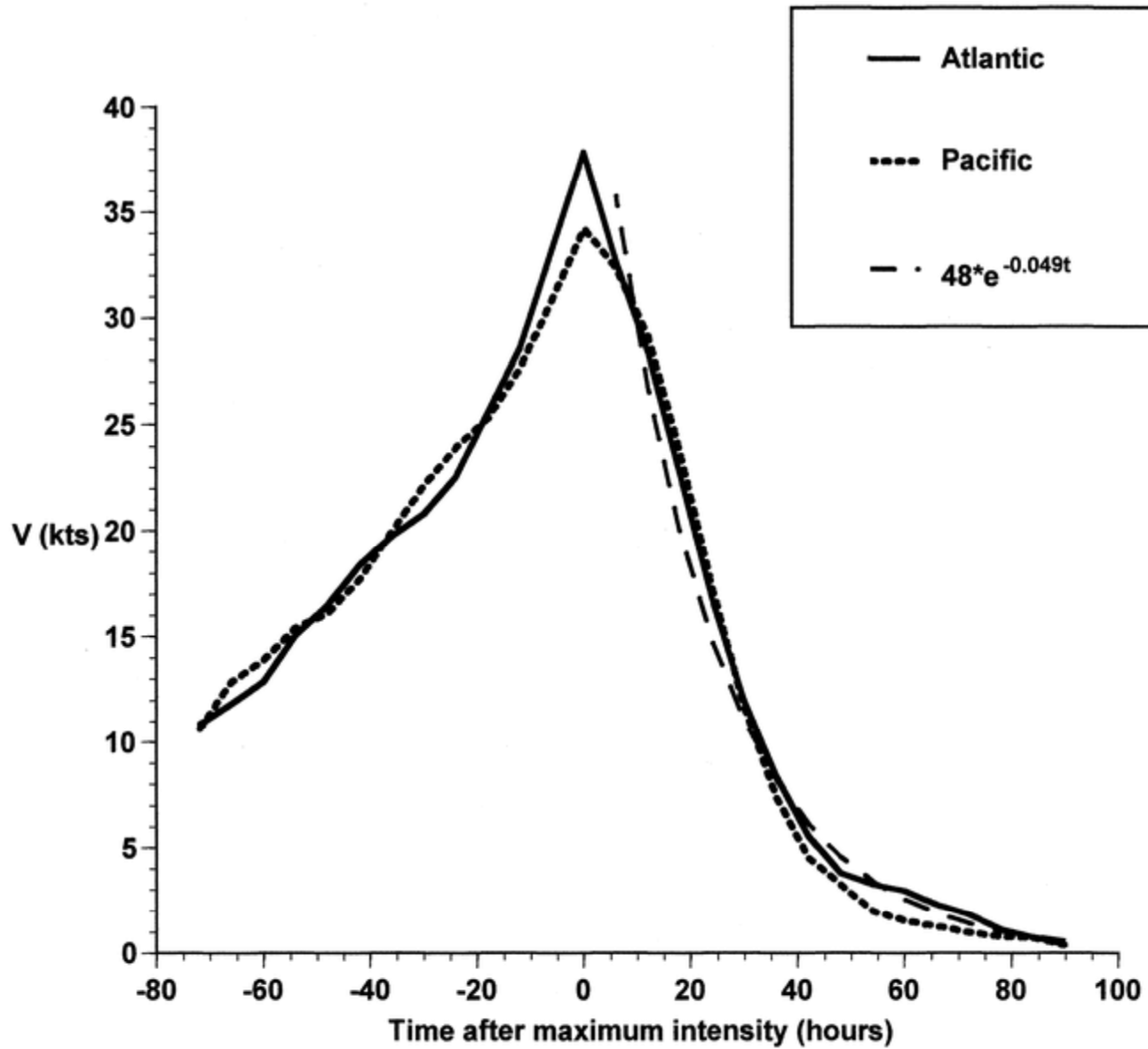
Evolution of Atlantic storms whose lifetime maximum intensity was limited by landfall



Evolution of Pacific storms whose lifetime maximum intensity was limited by landfall



Composite evolution of landfalling storms



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