

3.155J/6.152J Lecture 13: MEMS Lab Testing



Prof. Martin A. Schmidt
Massachusetts Institute of
Technology
10/31/2005



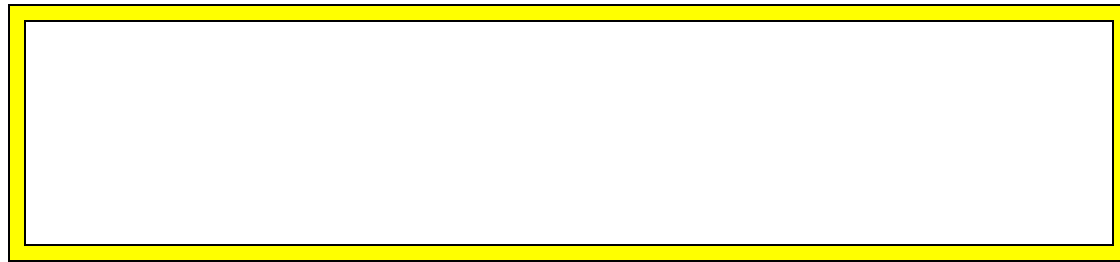
Outline

- Review of the Process and Testing
- Mechanics
 - Cantilever
 - Fixed-Fixed Beam
 - Second-order effects
 - Residual stress
 - Support compliance
- References
 - Senturia, *Microsystems Design*, Kluwer



The Process – Lab 1

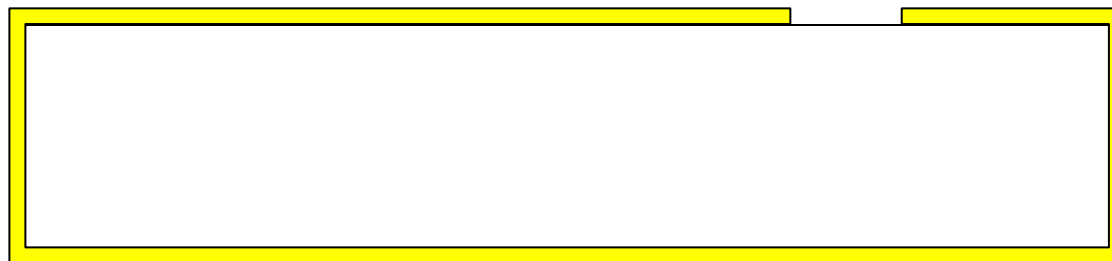
- Grow 1.0 μm of Si-Rich Silicon Nitride (SiN_x)
 - LPCVD Process (details to follow)
 - Characterize (UV1280)
 - Thickness
 - Refractive index





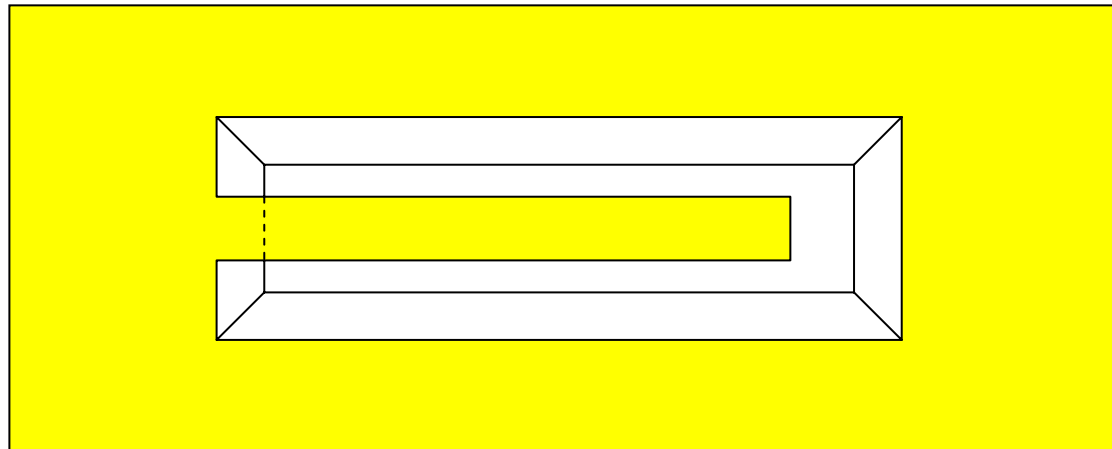
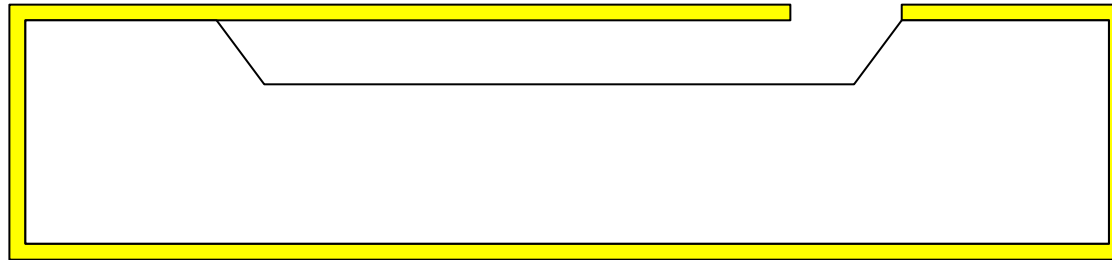
The Process – Lab 1

- Pattern Transfer
 - Deposit photoresist
 - Expose on contact aligner
 - Plasma etch using SF_6 chemistry
 - Strip resist



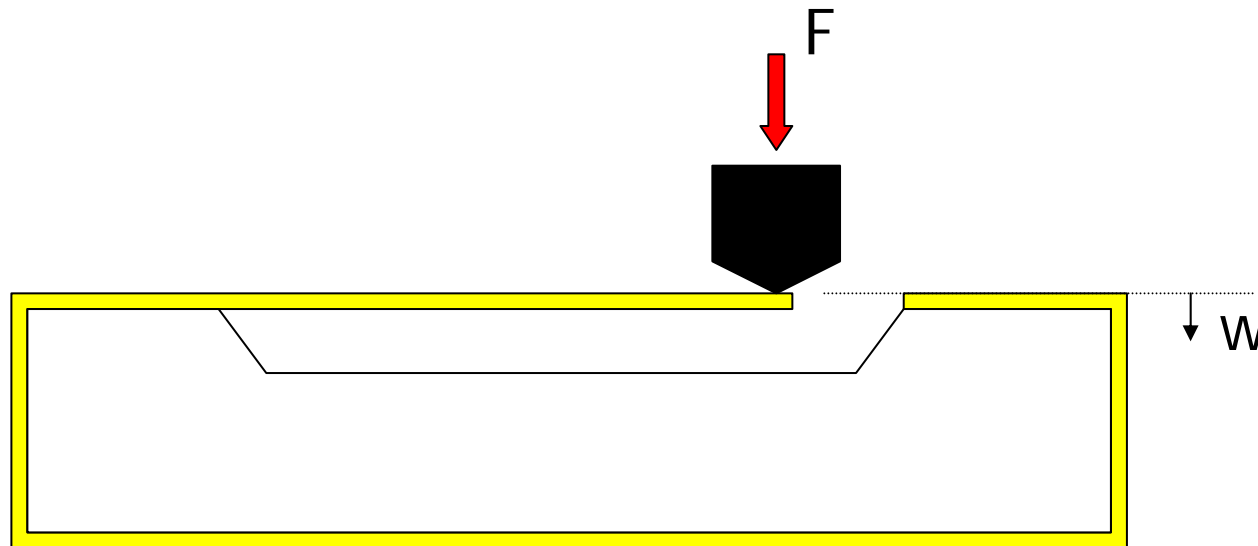
The Process – Lab 2

- KOH Undercut Etch
 - 20%, 80C



The Process – Lab 3

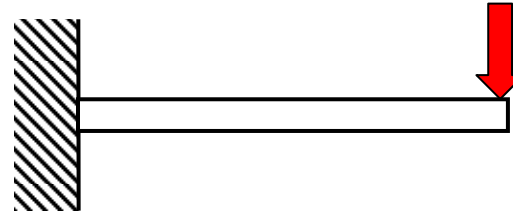
- Break the wafer into die
- Mount the die on a metal plate
- Test using the Hysitron Nanoindenter



Testing

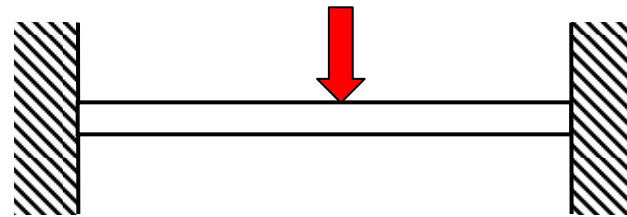
- Cantilever

- Young's Modulus



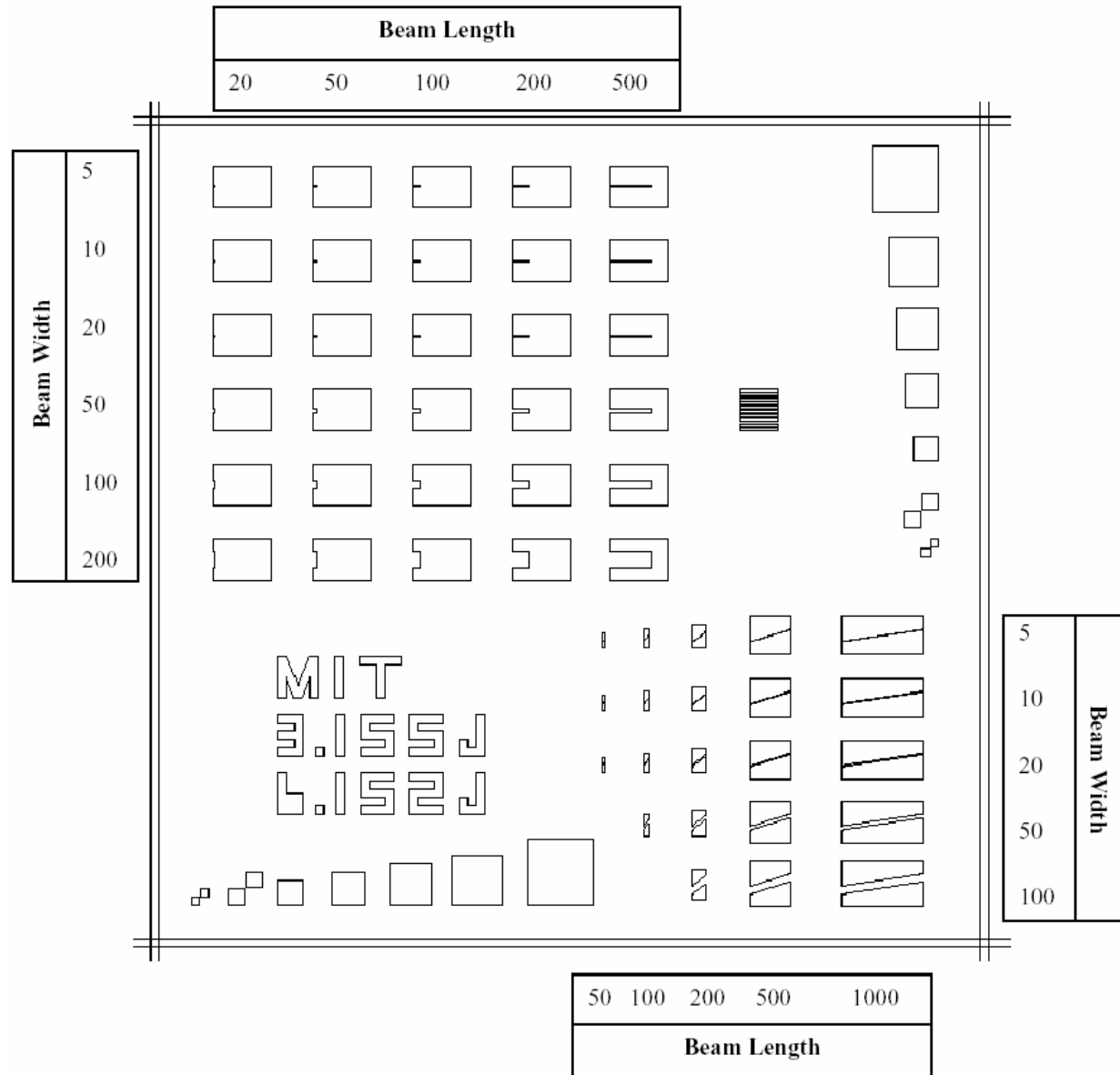
- Fixed-Fixed Beams

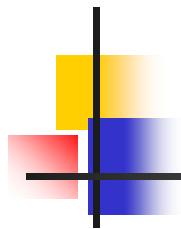
- Young's Modulus
- Residual Stress



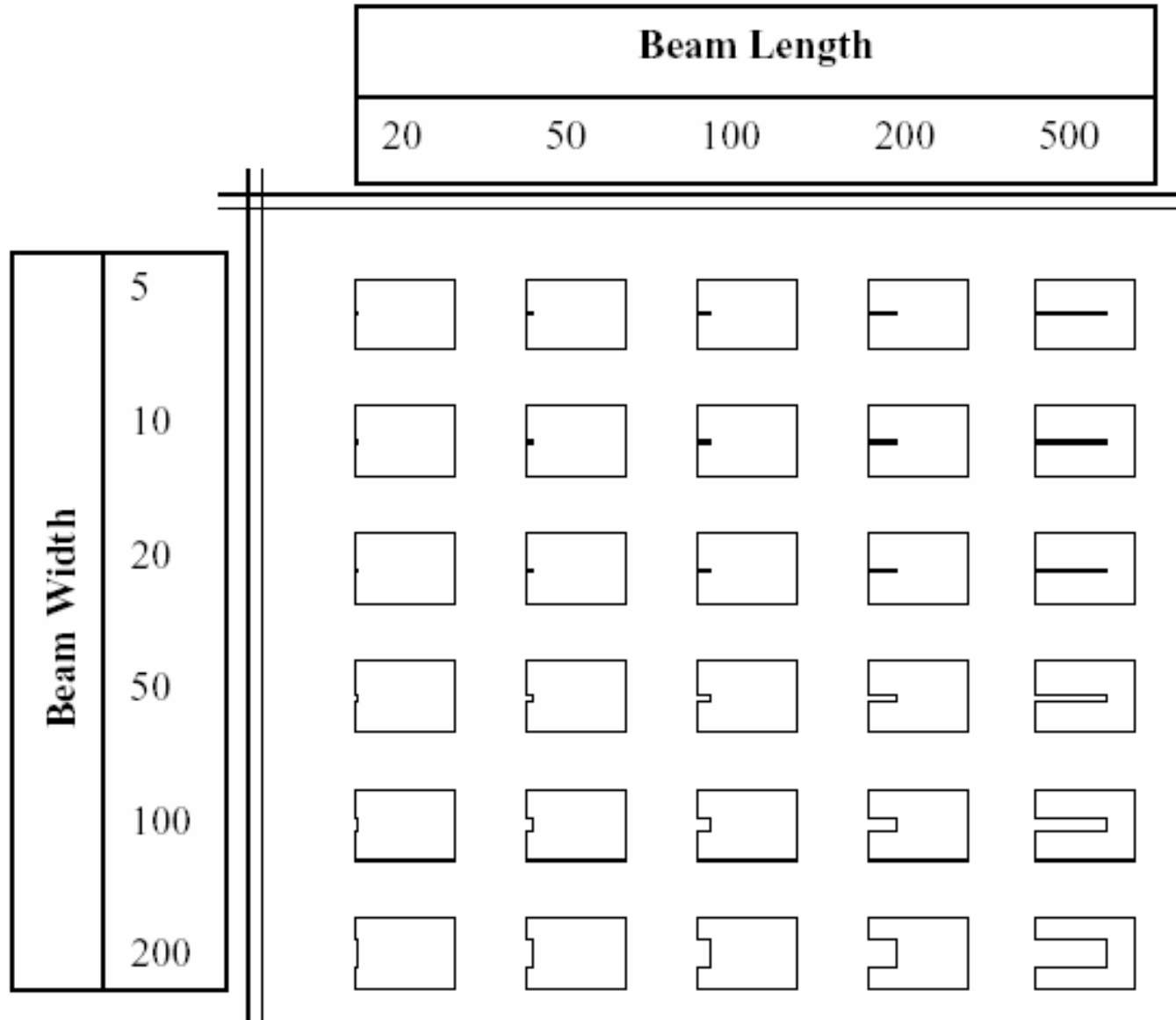


The Mask

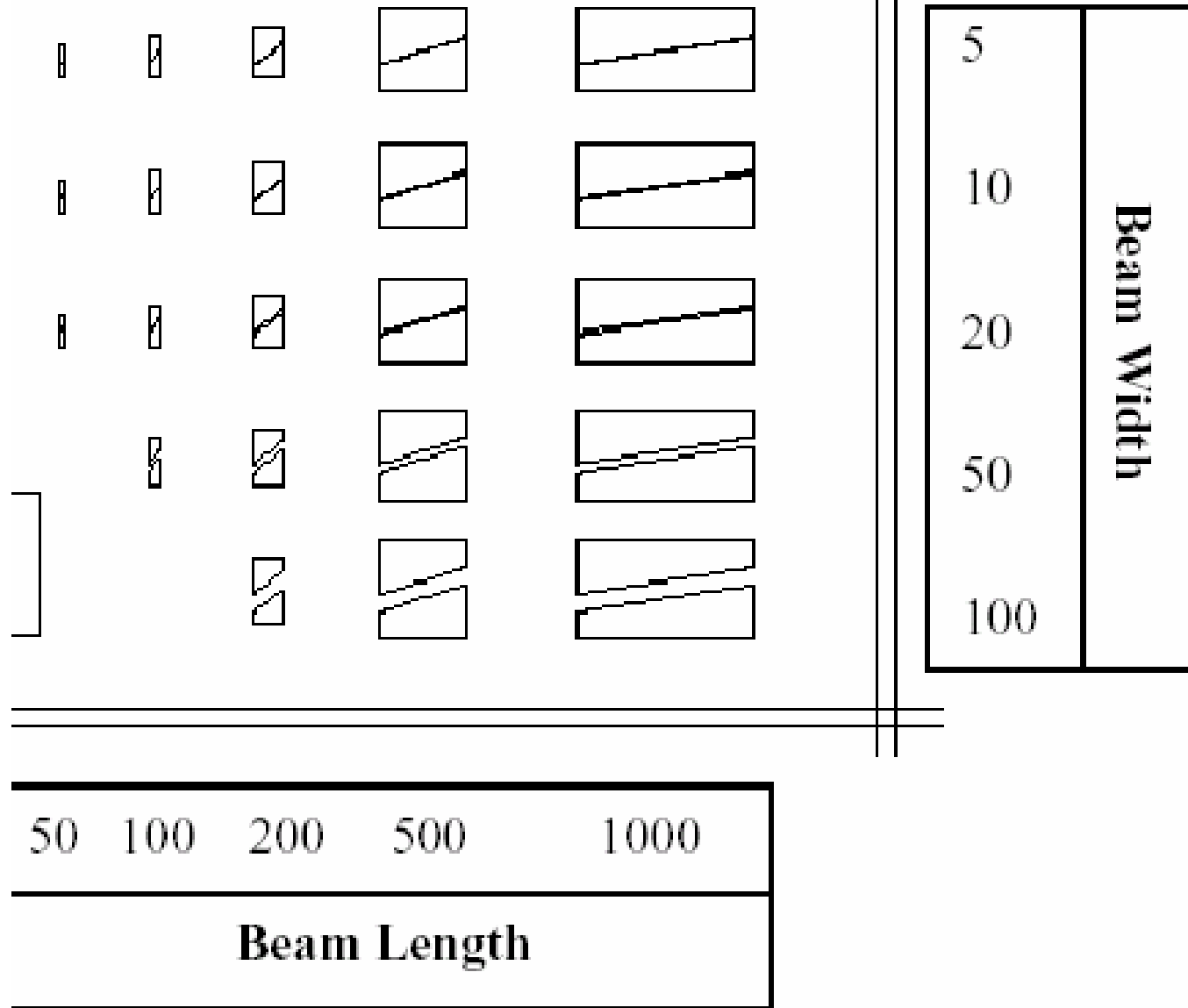


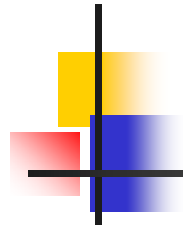


The Mask - Cantilevers



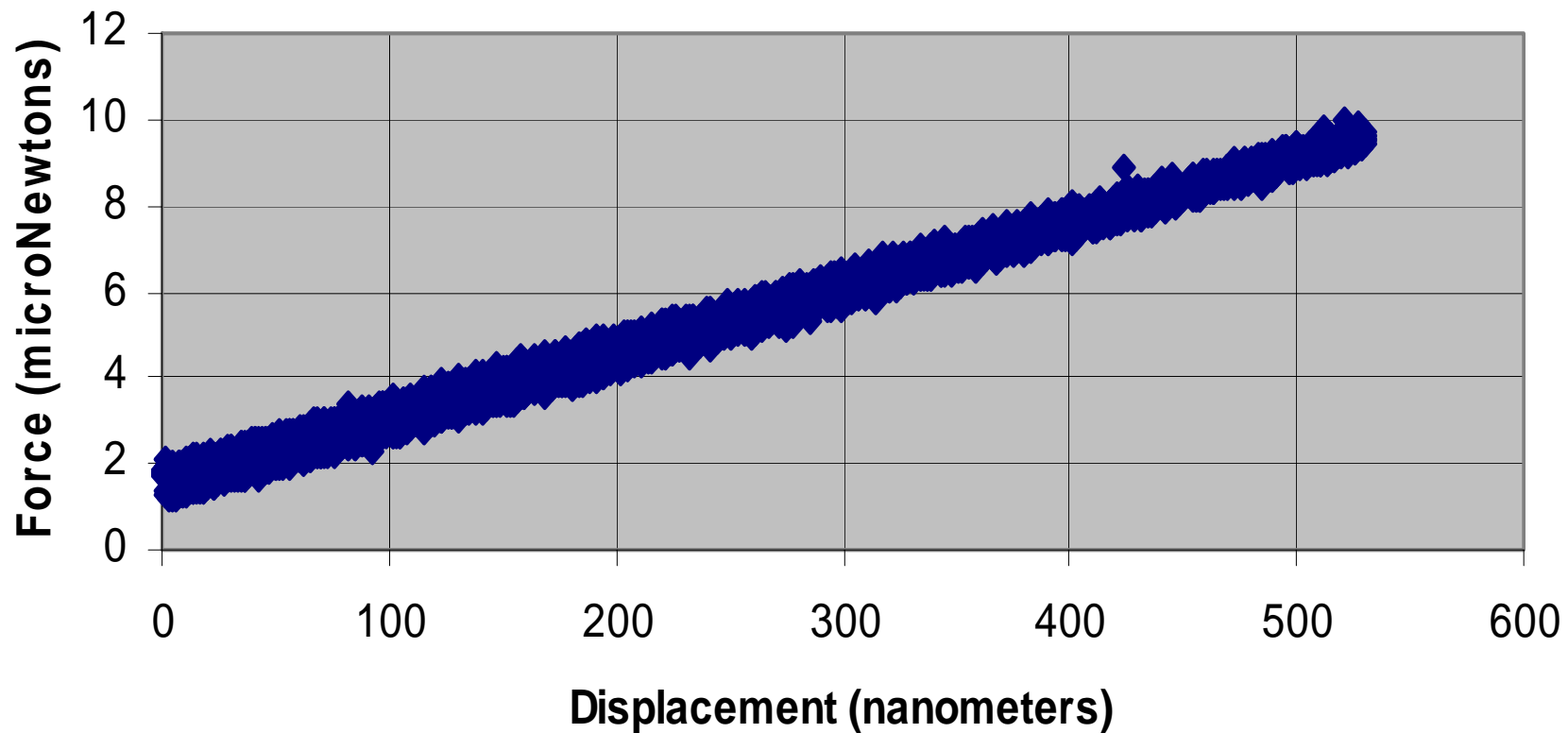
The Mask – Fixed-Fixed Beams





Cantilever Data

$$F = k x$$



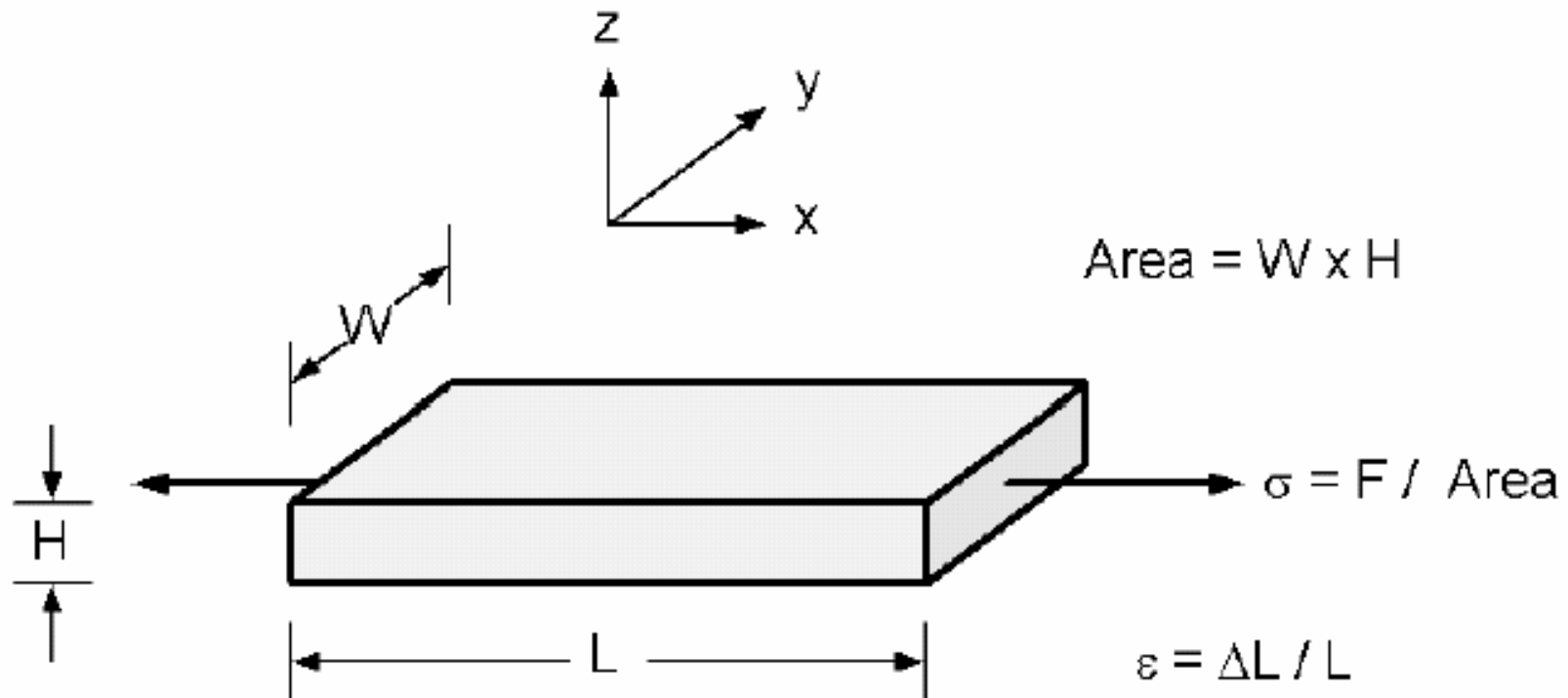
Force on a Beam

σ = stress = F / area (N/m², Pa, J/m³)

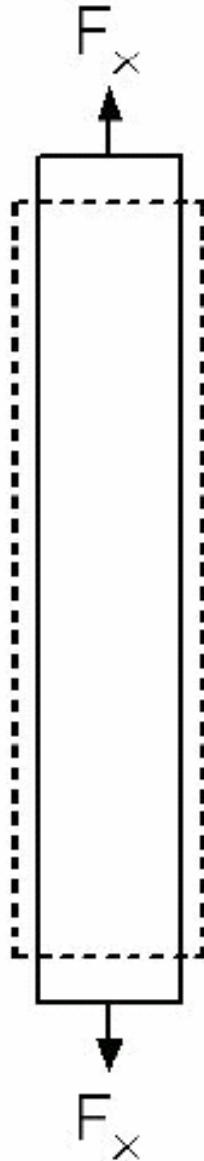
ε = strain = $\Delta L / L$ (unitless)

E = Young's Modulus (N/m², Pa, J/m³, ~160 GPa for Si)

$$\sigma = E \varepsilon$$



Uniaxial Stress



F_x = Force

σ = Force / (Normal Area)

ε = $\Delta L/L$

$\sigma = E \varepsilon$

E = Young's Modulus

ν = Poisson's ratio

$$\nu = -\frac{\text{transverse strain}}{\text{axial strain}} = -\frac{\varepsilon_y}{\varepsilon_x}$$

C.V. Thompson – 6.778J



Material Properties: Elastic/Plastic

Figure removed for copyright reasons.



Material Properties: Brittle

Figure removed for copyright reasons.

Differential Equation of Bending

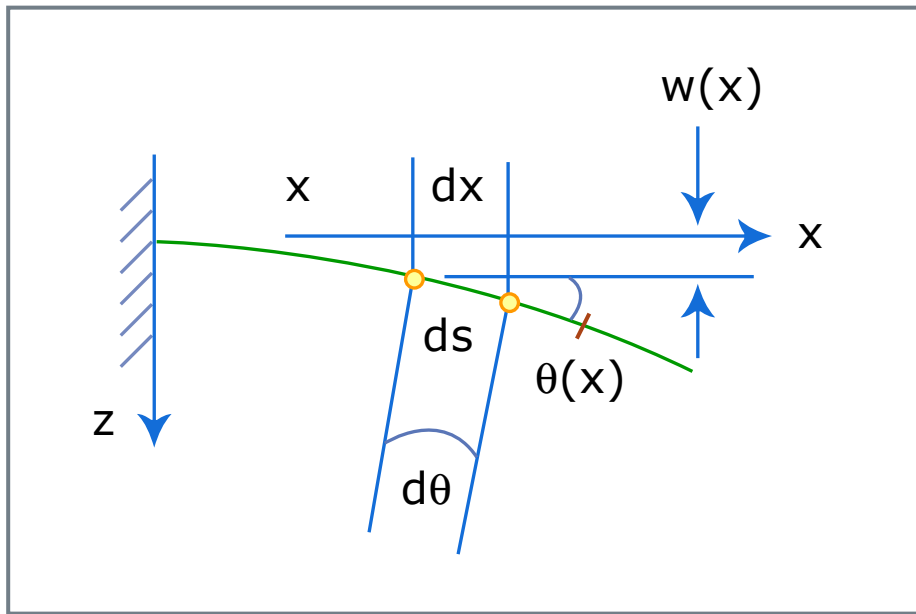


Figure by MIT OCW.

H = thickness

W = width

$$\frac{d^2w}{dx^2} = -\frac{M}{EI}$$

$$I = \left(\frac{1}{12} WH^3 \right)$$

Reference: Senturia, S.D. *Microsystems Design*. Norwell, MA: Kluwer Academic Publisher, 2001.

C.V. Thompson – 6.778J

3.155J/6.152J – Lecture 13 – Slide 16

Deflection of a Cantilever - 1

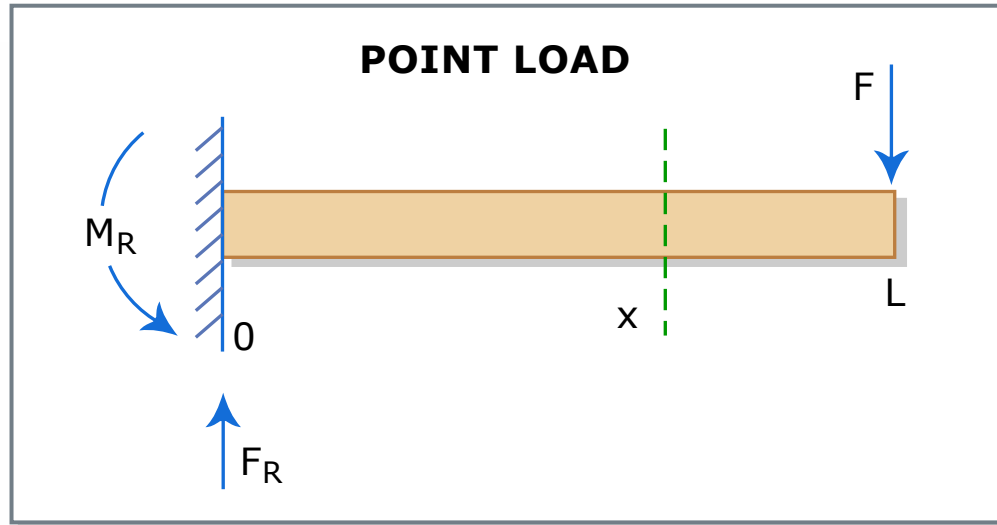


Figure by MIT OCW.

a point load F is applied at the end of a cantilever of length L .

The applied moment M_{applied} is balanced by the internal moment M as a function of x so $M_{\text{applied}}(x) = -M(x)$ and

$$M_{\text{applied}} = F(L-x) \text{ so } M = -F(L-x) \text{ so}$$

$$\frac{d^2w}{dx^2} = \frac{F}{EI}(L-x)$$

Ref: Senturia (Kluwer)
C.V. Thompson – 6.778J

3.155J/6.152J – Lecture 13 – Slide 17



Deflection of a Cantilever - 2

so solve

$$\frac{d^2w}{dx^2} = \frac{F}{EI}(L - x)$$

subject to

$$w(0) = 0$$

$$\left. \frac{dw}{dx} \right|_{x=0} = 0 \quad \text{zero slope at the support}$$

with the trial solution

$$w = A + Bx + Cx^2 + Dx^3$$

we find $A = B = 0$ and $C = \frac{FL}{2EI}$ and $D = -\frac{F}{6EI}$ so

$$w = \frac{FL}{2EI} x^2 \left(1 - \frac{x}{3L} \right)$$

Ref: Senturia (Kluwer)
C.V. Thompson – 6.778J



Deflection of a Cantilever - 3

the maximum deflection occurs at L so

$$w_{\max} = \left(\frac{L^3}{3EI} \right) F$$

so the spring constant for deflection ($F = k \delta x$) is

$$k_{\text{cantilever}} = \frac{3EI}{L^3} \quad \text{or with} \quad I = \left(\frac{1}{12} WH^3 \right)$$

W = width

H = thickness

L = length

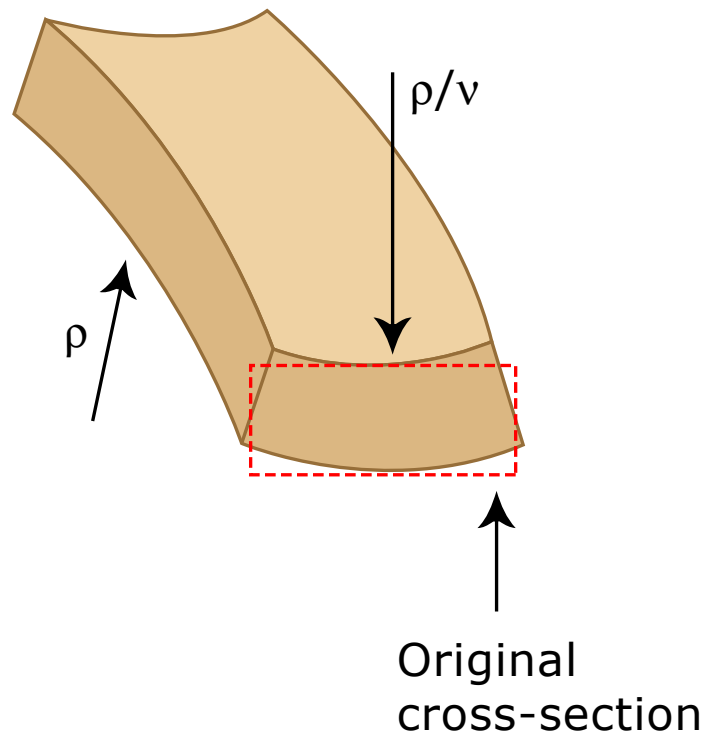
$$k_{\text{cantilever}} = \frac{EWH^3}{4L^3}$$

Ref: Senturia (Kluwer)

C.V. Thompson – 6.778J

Deflection of a Plate - 1

ANTICLASTIC CURVATURE



- Given axial strain ($\epsilon_x = \frac{z}{\rho}$)
- Poisson effect leads to transverse strain ϵ_y given by $\epsilon_y = -\nu\epsilon_x$ where ν is Poisson's ratio (unitless and about 1/3 for most materials)
- So ($\epsilon_y = \frac{\nu}{\rho} z$)
- More important as $W \rightarrow L$ (beams approach plates)

Figure by MIT OCW.

Ref: Senturia (Kluwer)
C.V. Thompson – 6.778J



Deflection of a Plate - 2

$$\varepsilon_x = \frac{\sigma_x - \nu\sigma_y}{E}$$

But ε_y is constrained to be zero

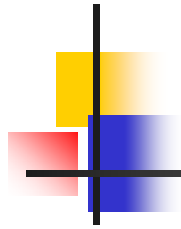
$$\Rightarrow 0 = \varepsilon_y = \frac{\sigma_y - \nu\sigma_x}{E}$$

\Downarrow

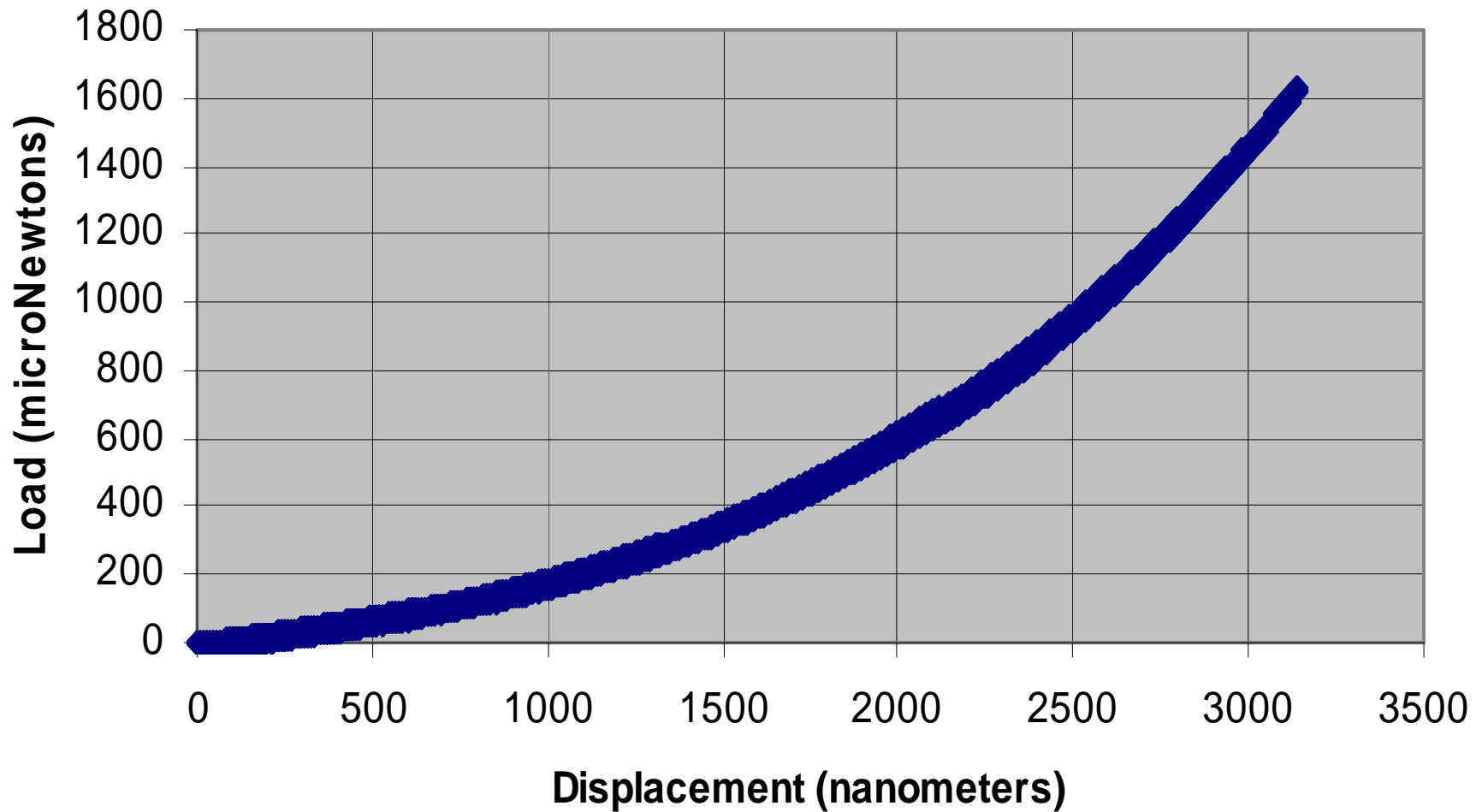
$$\sigma_x = \underbrace{\left(\frac{E}{1 - \nu^2} \right)}_{\text{Plate Modulus}} \varepsilon_x$$

Replace Modulus(E)
with Plate Modulus

Ref: Senturia (Kluwer)



Fixed-Fixed Beam





Fixed-Fixed Beam: Large Displacement

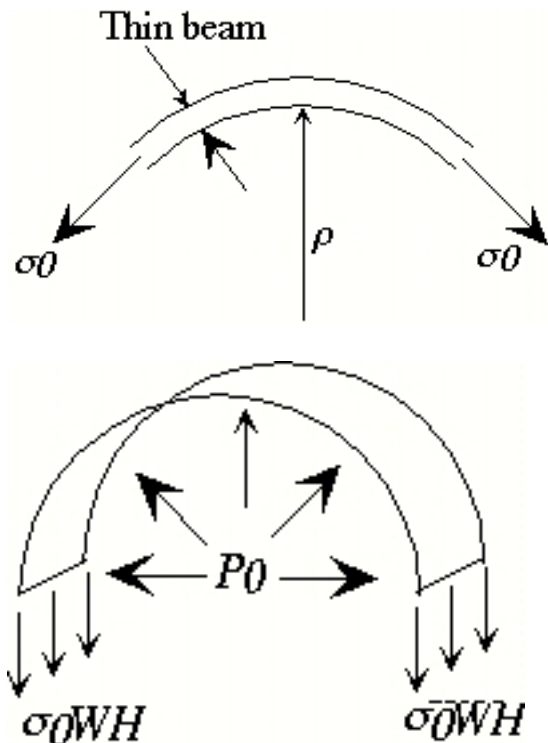
- Beam stretches under large displacement
 - Becomes 'stiffer'
- Solved by Energy Methods
 - $C = W$

$$F = \left(\frac{\pi^4}{6}\right) \left[\frac{EWH^3}{L^3}\right] c + \left(\frac{\pi^4}{8}\right) \left[\frac{EWH}{L^3}\right] c^3$$

Ref: Senturia (Kluwer)

Residual Axial Stress in Beams

- Residual axial stress in a beam contributes to its bending stiffness
- Leads to the Euler beam equation



$$2\rho WP_0 = 2\sigma_0 WH$$

$$\Rightarrow P_0 = \frac{\sigma_0 H}{\rho}$$

which is equivalent to a distributed load

$$q_0 = P_0 W = \sigma_0 WH \frac{d^2 w}{dx^2}$$

Insert as added load into beam equation :

$$EI \frac{d^4 w}{dx^4} = q + q_0$$

$$EI \frac{d^4 w}{dx^4} - \sigma_0 WH \frac{d^2 w}{dx^2} = q$$

Ref: Senturia (6.777)



Effect of stress on stiffness

Figure removed for copyright reasons.

Graph found in Senturia, S.D. *Microsystems Design*. Norwell, MA: Kluwer Academic Publisher, 2001.

Ref: Senturia (6.777)



Effect of Residual Stress

- Not an issue in cantilevers
- For a point load, F , in the center of a bridge

$$F = \left\{ \left(\frac{\pi^2}{2} \right) \left[\frac{\sigma_0 W H}{L} \right] + \left(\frac{\pi^4}{6} \right) \left[\frac{E W H^3}{L^3} \right] \right\} c + \left(\frac{\pi^4}{8} \right) \left[\frac{E W H}{L^3} \right] c^3 \quad (10.70)$$

- Important when

$$\sigma_0 \approx \frac{E H^2}{L^2}$$

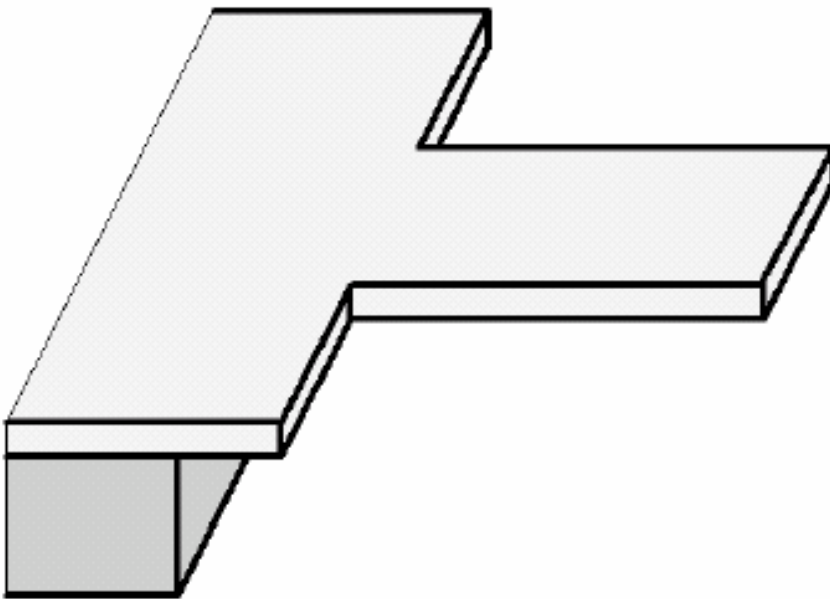
Ref: Senturia (Kluwer)

Compliant Supports

In the forgoing we have assumed that the beam support was ideal, i.e.

$$\left. \frac{dw}{dx} \right|_{x=0} = 0$$

This is often not the case. A common cause for support compliance is etch undercut. This can be rigorously dealt with mathematically, but approximate treatments are often adequate.



One approach is to introduce an effective length through a length correction, which is empirically fit to observations:

$$L = L_{\text{measured}} + L_{\text{correction}} = L_m + L_c$$

C.V. Thompson – 6.778J

3.155J/6.152J – Lecture 13 – Slide 27



MEMS Lab Report

- Report Young's Modulus extracted from
 - Cantilevers
 - Fixed-Fixed Beams
- Explain differences from ideal theory
- Compare to literature values for mechanical properties
- Assess the effects of:
 - Residual stress
 - Estimate from measurements
 - Experimental error
 - Compliant supports
 - Beam versus Plate
 - Others....